



Optical Interface for MSC.Nastran

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Sigmadyne, Inc



Optical Interface for MSC.Nastran

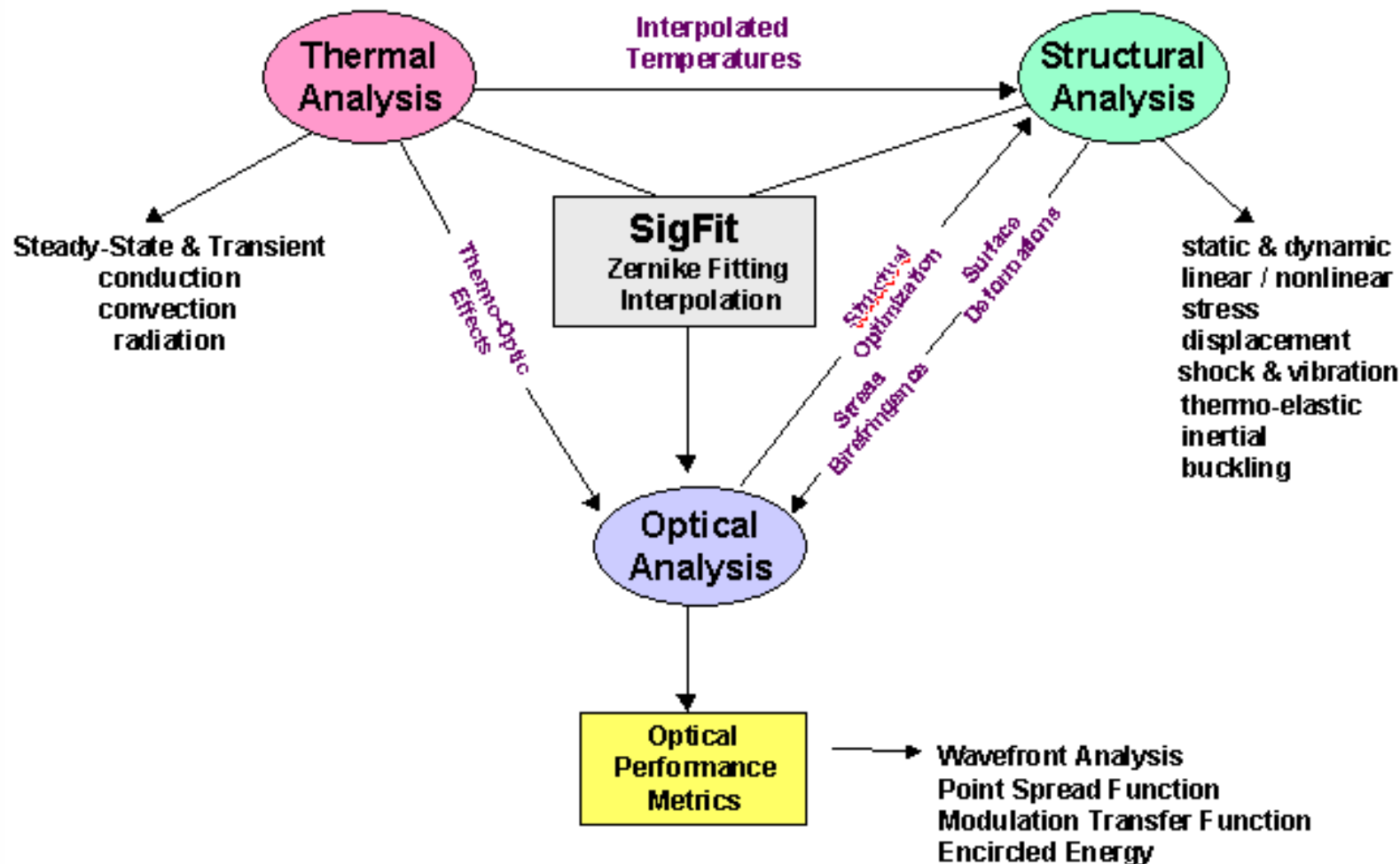
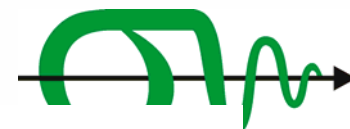


Outline of Presentation

- Integrated analysis procedure
- Surface distortions
- Thermo-optic effects
- Stress-optic effects
- Random response
- Adaptive (deformable) optic analysis
- System analysis
- Opto-Mechanical Optimization
- Summary



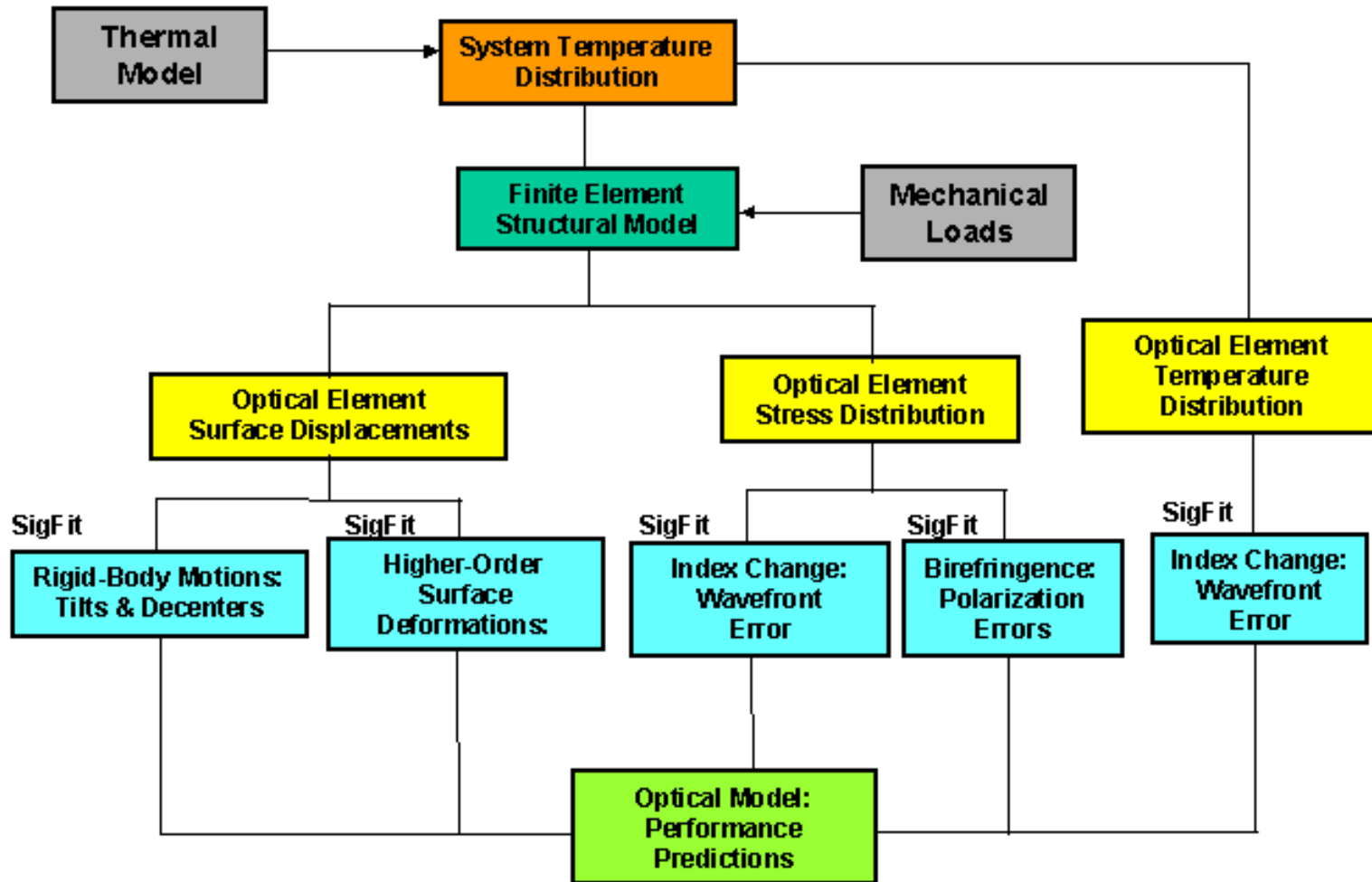
Integrated Analysis of Optical Systems

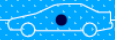


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Analysis Flow for Optical Performance





Input to Optics Programs



Can NOT import FE results directly

- displacements, temperature, stress

Can pass FE results only as

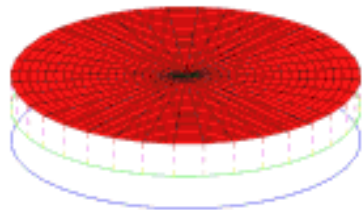
- “rigid body” motion (6 DOF per surface)
- Zernike/other polynomials (fit to results)
- Interferogram rectangular array (Hit Map)

SigFit supports all above forms

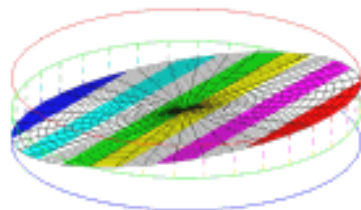
- Code V, Oslo, Zemax formats



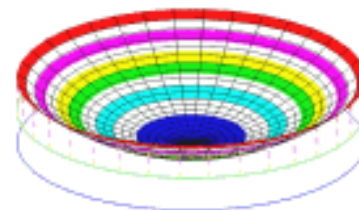
Zernike Polynomials



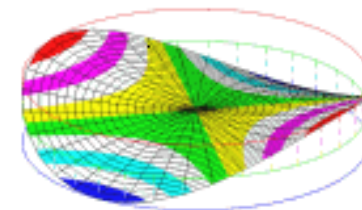
Bias/Piston



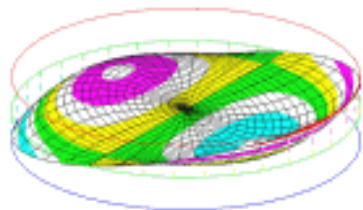
Tilt



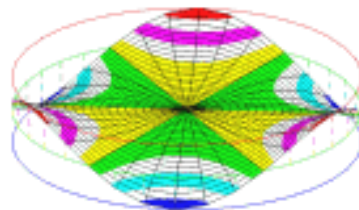
Power/Defocus



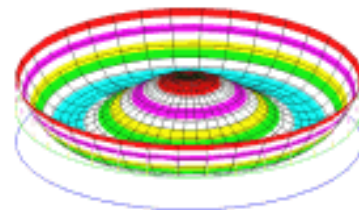
Pri-Astigmatism



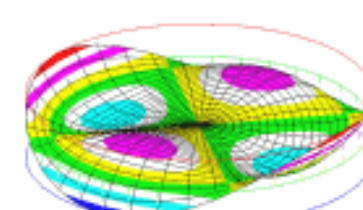
Pri-Coma



Pri-Trefoil



Pri-Spherical

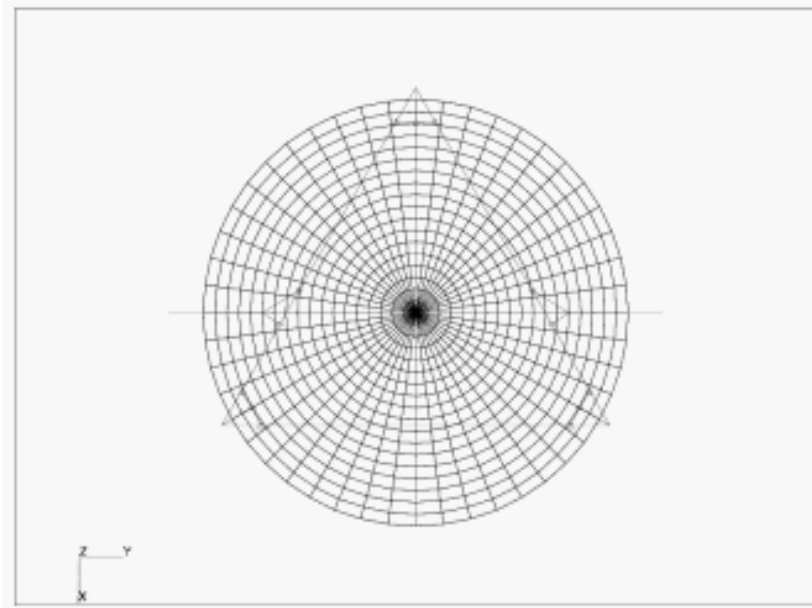


Sec-Astigmatism

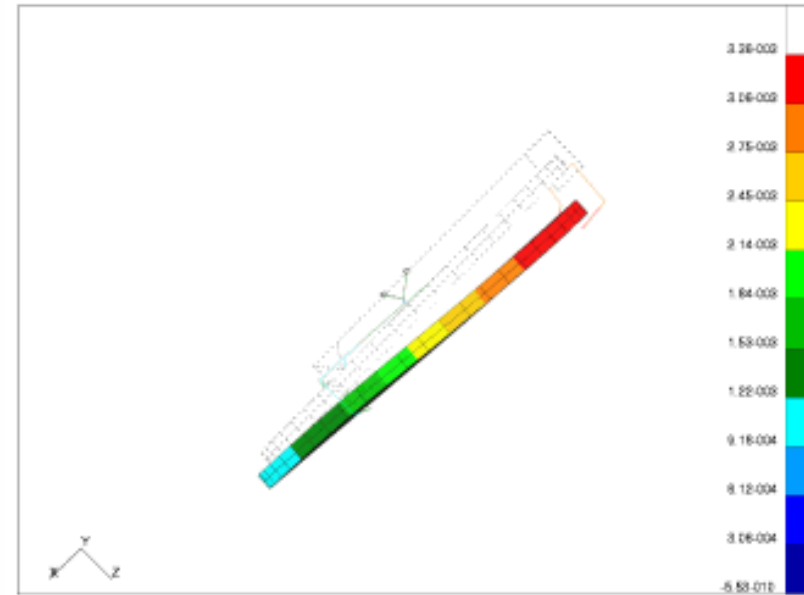
$$\Delta Z(\rho, \Theta) = A_{00} + \sum_{N=2}^{\infty} A_{N0} R_0^N(\rho) + \sum_{N=1}^{\infty} \sum_{M=1}^{\infty} R_M^N \left[A_{NM} \cos(M\Theta) + B_{NM} \sin(M\Theta) \right]$$



Structural Distortion



Mirror on Delta Frame

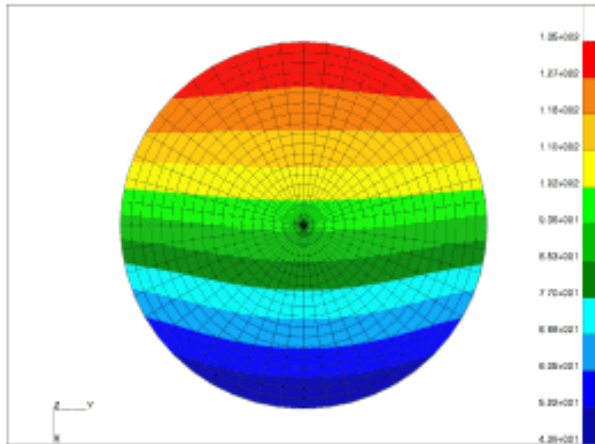


Deformed in 1g

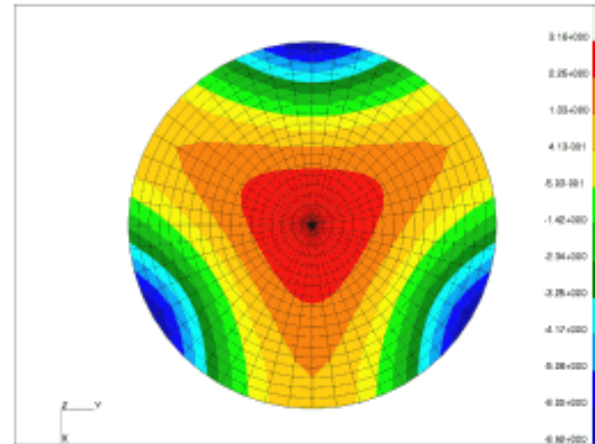
FE deformation dominated by “rigid body” motion which will be aligned out of the system



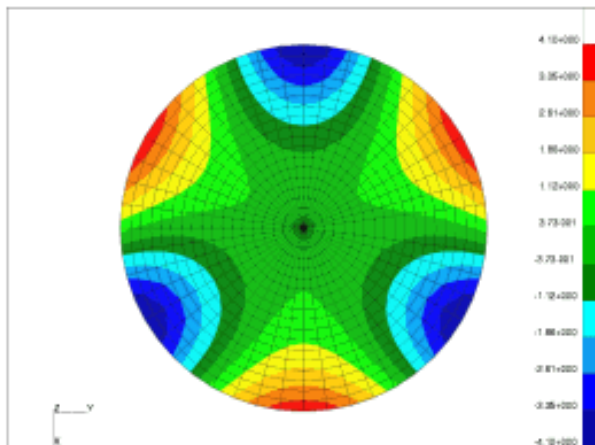
Structural Distortion



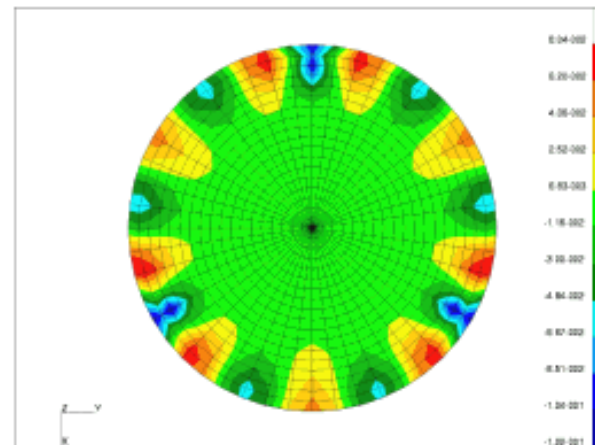
FE Raw Displacement (Normal) RMS=95 μ



Best-Fit Plane Removed in SigFit RMS=2.3 μ



BFP and Power Removed in SigFit RMS=1.6 μ



All Terms Removed in SigFit RMS=0.03 μ



Structural Distortion



Sigmadyne, Inc.

SigFit Version=v2003-r1

Order			Aberration	Magnitude	Phi	Residual	Residual
K	N	M		(Waves)	(Deg)	RMS	P-V
			Input(wrt zero)			95.6034	91.1636
1	0	0	Bias	92.29817	.0	24.9243	91.1636
2	1	1	Tilt	49.61448	179.9	2.2775	10.0795
3	2	0	Power (Defocus)	-2.81611	.0	1.5887	8.1731
4	2	2	Pri Astigmatism	.03751	89.8	1.5886	8.1791
5	3	1	Pri Coma	.01434	-180.0	1.5886	8.1862
6	3	3	Pri Trefoil	4.43376	0.0	.2369	1.3379
7	4	0	Pri Spherical	.33960	.0	.1782	1.1849
8	4	2	Sec Astigmatism	.00891	0.0	.1781	1.1890
9	4	4	Pri Tetrafoil	.01092	0.0	.1781	1.1760
10	5	1	Sec Coma	.00038	0.0	.1781	1.1764
11	5	3	Sec Trefoil	.43847	-60.0	.1203	.7565
12	5	5	Pri Pentafoil	.00226	-.1	.1203	.7596
13	6	0	Sec Spherical	-.00403	.0	.1203	.7596
14	6	2	Ter Astigmatism	.00037	-90.0	.1203	.7599
15	6	4	Sec Tetrafoil	.00124	0.0	.1203	.7599
16	6	6	Pri Hexafoil	.42821	-30.0	.0379	.3101

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Structural Distortion



SigFit separates FE displacements:

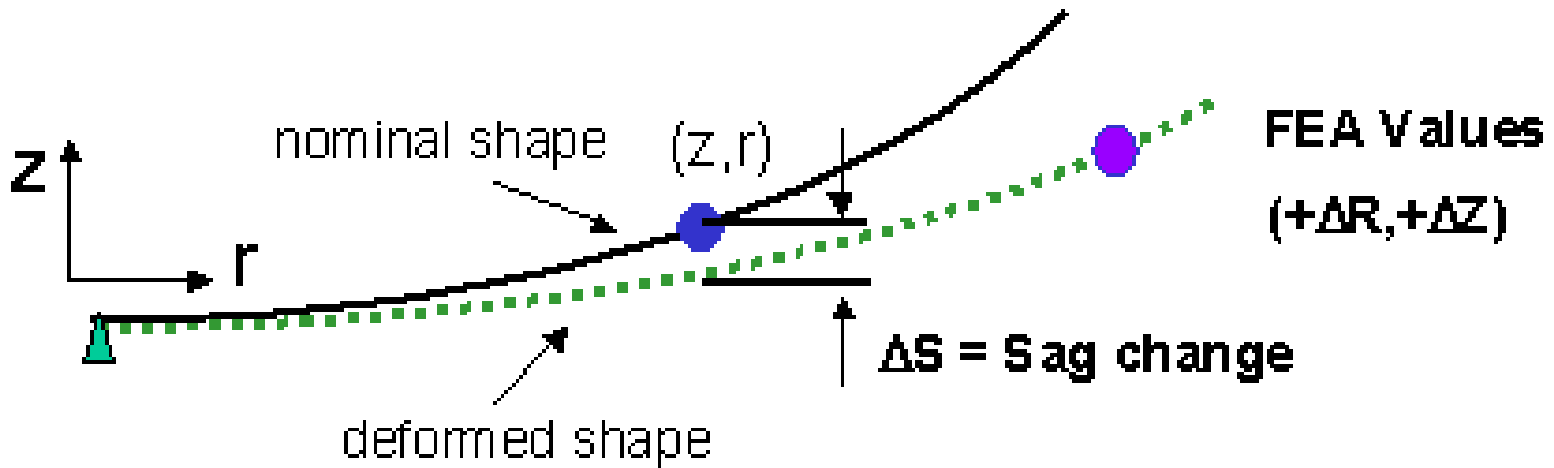
- Pointing error (corrected by repointing)
 - if system has alignment capability
- Focus error (corrected by refocusing)
 - if systems has focus capability
- Elastic wavefront error (uncorrectable)
 - requires adaptive mirror to correct

SigFit passes FE displacements to optic code

- Writes Zernikes in optic code's format
- Using optic code's ordering and normalization



Radial Correction



FEA ΔZ displacement does NOT represent surface Sag

SigFit calculates Sag as the combined effect of ΔZ and ΔR



Interpolation Hit Map \Leftrightarrow FE Model



Interferometric testing creates Hit Maps

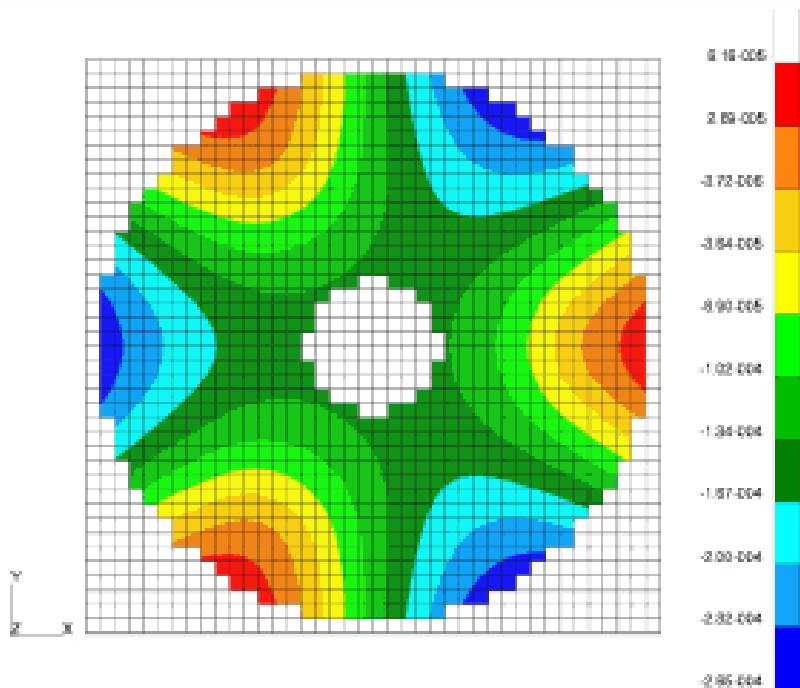
- rectangular array of data

SigFit interpolates between FE Models and Interferogram Arrays (Hit Maps)

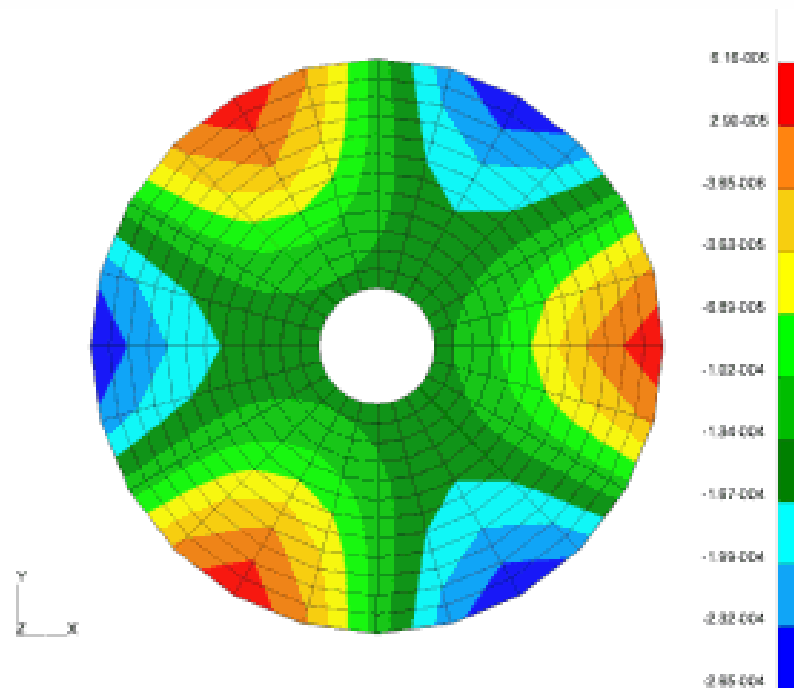
- Output FE analysis data to test systems
- Compare test and analysis (point-to-point)
- Create analysis backouts for ground tests
- Import test data for adaptive correction
- Used when Zernikes are a poor fit to deformations



Interpolation Hit Map \Leftrightarrow FE Model

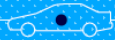


HitMap Contours



FE Model Contours

SigFit passes data between test interferograms and FE models using FE shape functions for interpolation



Thermo-Optic Effect



Temperature causes change in index (n)

- index changes cause optical pathlength changes
- OPD = Optical Path Difference

SigFit calculates OPD due to dn/dT

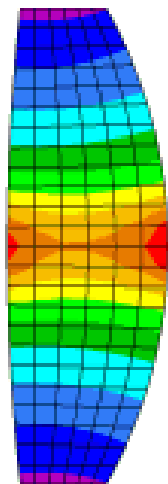
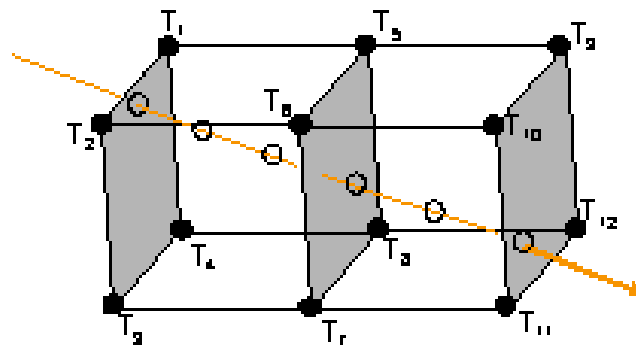
- Reads MSC.Nastran thermal results
- Integrate through the optic along ray paths
- Calculates OPD
 - Fit Zernikes to OPD, write in optics format
 - Interpolate to HitMap, write in optics format
 - Supports CodeV, Zemax, Oslo formats



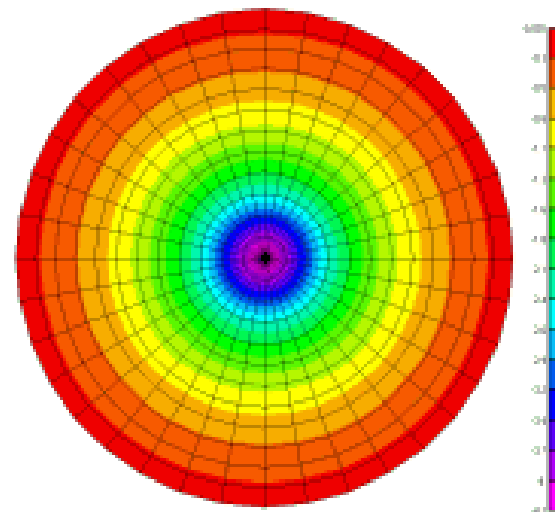
Thermo-Optic Effect



$$OPD = \sum_{n=1}^{n=total} \frac{Dn}{Dt} \Delta T_n L_n$$



Lens Temperature Distribution



Lens OPD Map



Stress-Optic Effects



Stress causes changes in index ($dn/d\sigma$)

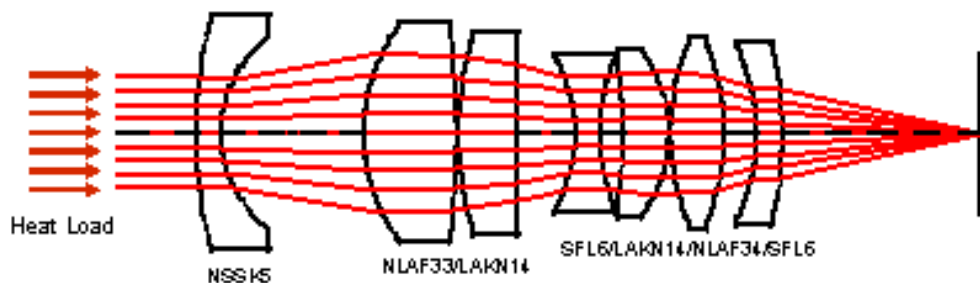
- index changes cause pathlength changes (OPD)
- birefringence cause polarization changes (Δ OPD)

SigFit calculates OPD & birefringence

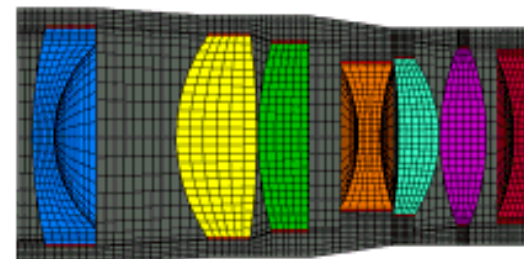
- Reads MSC.Nastran stress results
- Integrates through the optic
 - shape function interpolation through elements
- Calculates OPD & Birefringence
 - Fit Zernikes to OPD, write in optics format
 - Interpolate to HitMap, write in optics format
 - Supports CodeV, Zemax, Oslo formats



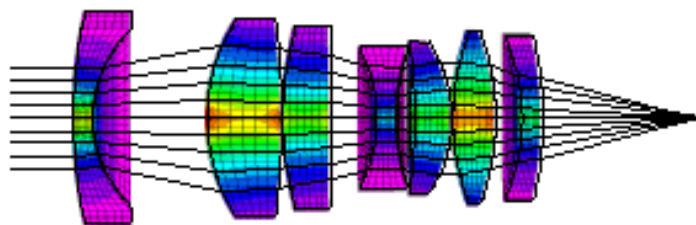
Combined Stress & Thermal effects



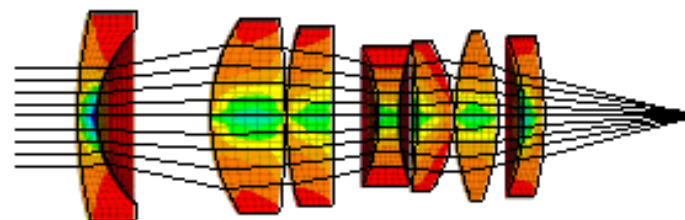
Optical Model



FEA Model



Temperature Field



Stress Field

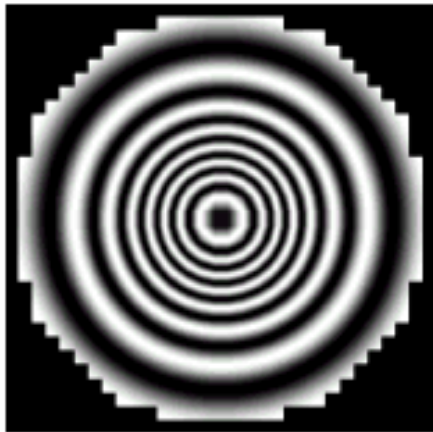
SigFit calculates the OPD effect for dn/dT and $dn/d\sigma$ which can be combined with surface distortions and passed to an optics code



Combined Stress & Thermal effects



**Thermo-Elastic
Interferogram Map**



**rms = 1.7
p-v = 7.6**

**Stress-Induced
Interferogram Map**



**rms = 0.4
p-v = 1.2**

**Thermo-Optic
Interferogram Map**



**rms = 1.9
p-v = 8.5**

SigFit data passed to Code V. Above results from Code V



Dynamic Analysis



FEA random response results

- optical surface responses are all RMS values (>0)
- cannot distinguish rigid-body from elastic motion
- cannot differentiate pointing from wavefront errors



All RB motion, No elastic distortion



No RB motion, All elastic distortion



Dynamic Analysis



SigFit calculates dynamic response

- reads MSC.Nastran mode shapes
- decomposes mode shapes into
 - rigid body and elastic components
- calculates harmonic & random response
 - uses modal analysis methods
 - reports pointing error (rigid body) response
 - reports wavefront error (elastic) response



Adaptive (Deformable) Optic Analysis

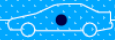


Adaptive optics used to improve performance

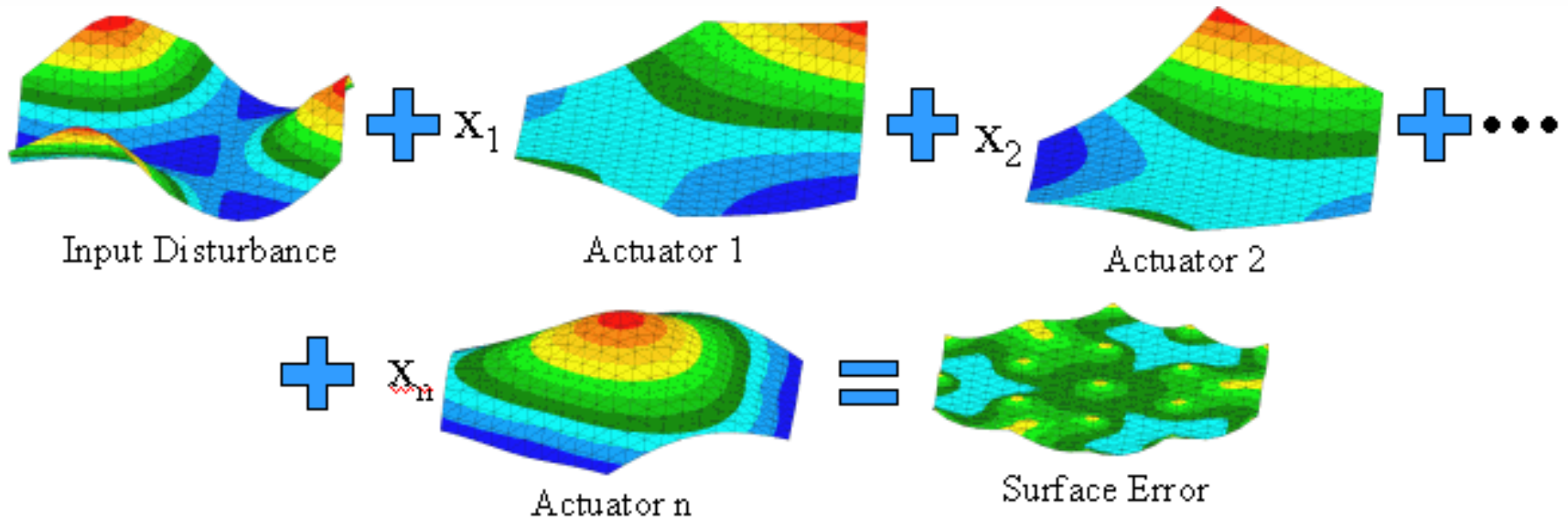
- Cancel atmospheric turbulence
- Correct fabrication / mounting errors
- Correct for thermal distortions
- Correct for mechanical distortions

SigFit calculates adaptive correction

- Finds actuator motions required to minimize RMS
- Calculates corrected surface and actuation forces
- Outputs resulting surface in optics format



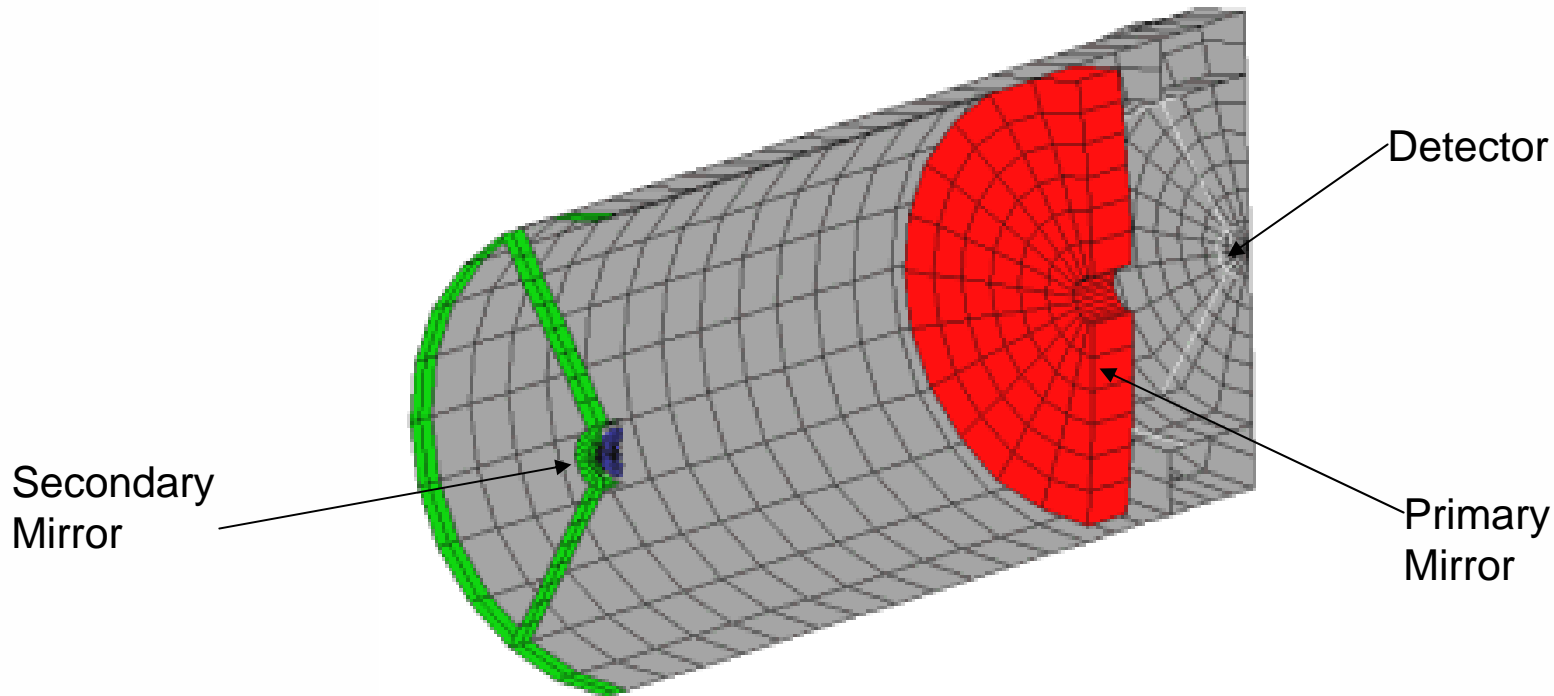
Adaptive (Deformable) Optic Analysis



- SigFit supports a very general adaptive analysis capability
 - force and/or displacement actuators
 - test and/or analysis input disturbance
 - bounded or unbounded solutions (actuator limits)



Adaptive (Deformable) Optic Analysis



Simple Telescope with Adaptive Primary Mirror
Cut-away view showing inside



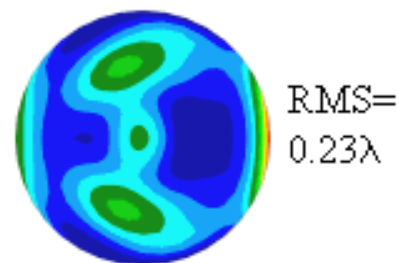
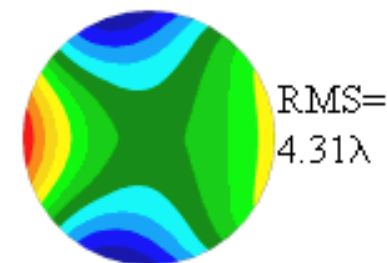
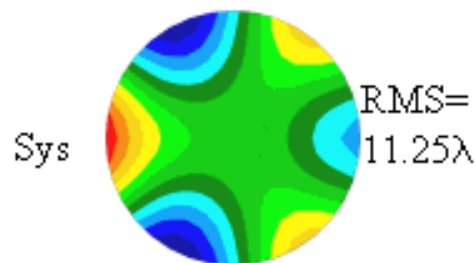
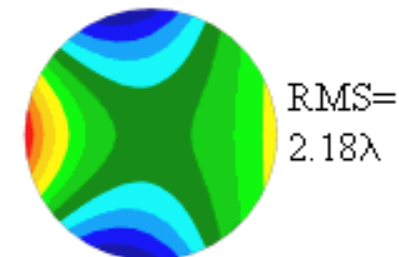
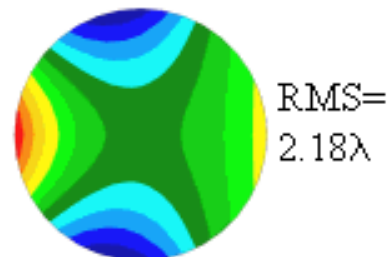
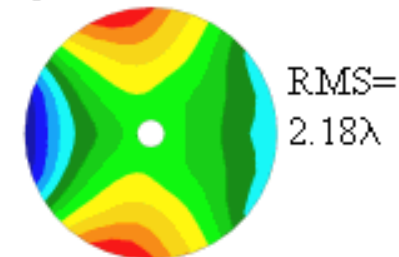
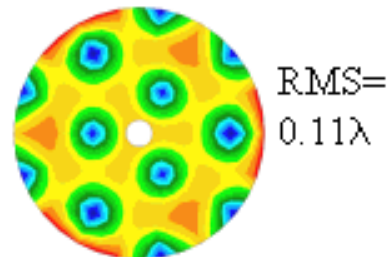
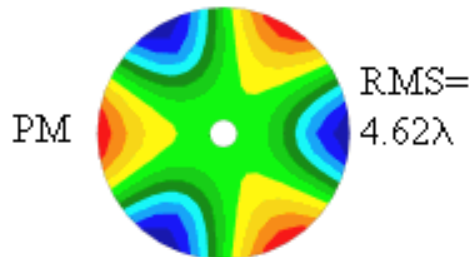
Adaptive (Deformable) Optic Analysis



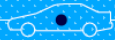
No Correction

PM Correction

Sys Correction



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System Analysis

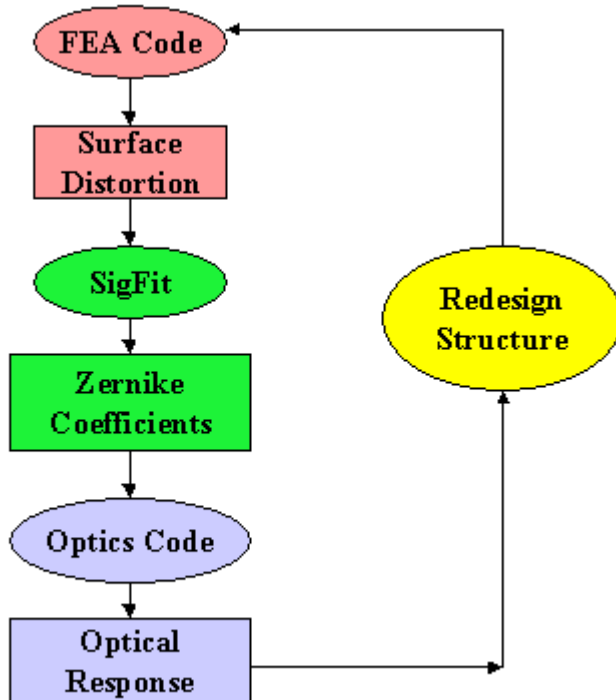


SigFit supports system analysis

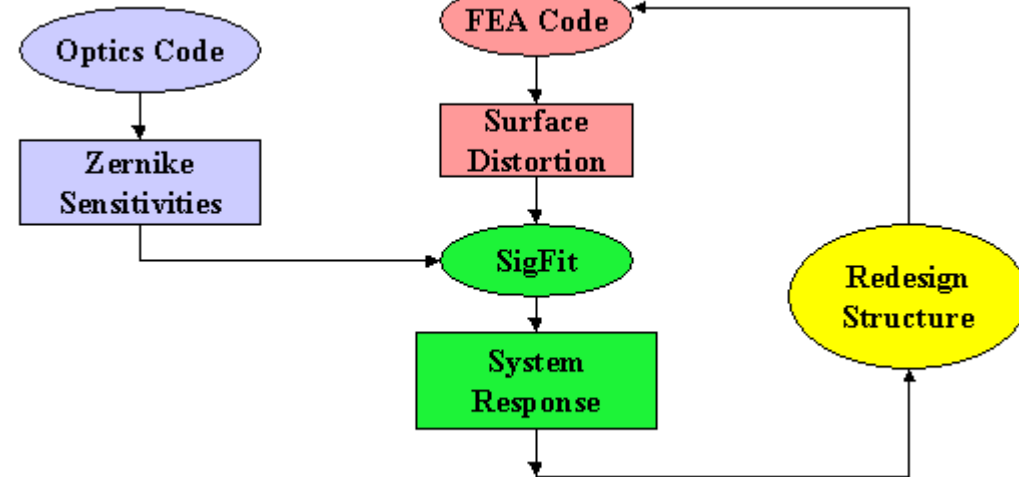
- Uses Zernike sensitivities from optics program
 - Input unit Zernikes at each surface (use script)
 - Create Matrix of Zernike responses at exit pupil
- SigFit will calculate system response
 - Fit Zernikes on each surface to FE results
 - Multiply by sensitivity matrix to get resulting response
 - Used for system analysis/ adaptive/ dynamic response
- Provides much faster design iteration



System Analysis

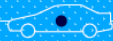


Old Design Process



New Design Process

Mechanical design process involves only the mechanical engineer.
 There is no trading of data back and forth during design cycle



Opto-Mechanical Optimization



SigFit supports MSC.Nastran SOL 200

- Writes Surface RMS or Peak-to-Valley after Zernike fit as **DRESP2**
 - Can then be used as a constraint or as the objective in SOL 200
 - Especially useful in the optimum design of large light-weight mirrors
 - Well established and documented procedure
- Writes Surface/System wavefront response as **DRESP3**
 - Writes necessary DRESP1 and DRESP3 in a preprocessing step
 - Called by DRESP3 to calculate individual surface or total system response
 - Especially useful in system level optimization with adaptive control
 - New feature discussed in Greg Michels' paper
- Allows optical performance measures to be used in structural optimization



Optical Interface for MSC.Nastran



References at www.sigmadyne.com

- Several recent papers (download)
 - Technical details on all topics in this talk
- SigFit documentation (download)
 - Reference Manual
 - Examples Manual
 - Example I/O files

Short Course & Book from SPIE:

- [Integrated Optomechanical Analysis](#)