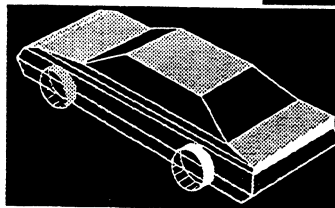
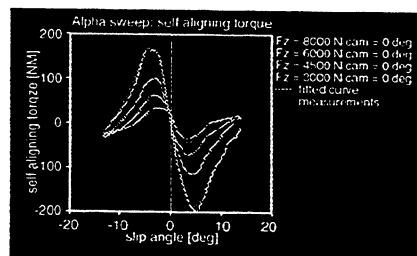
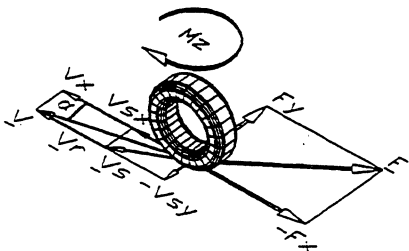


Delft-Tyre a design and analysis tool...



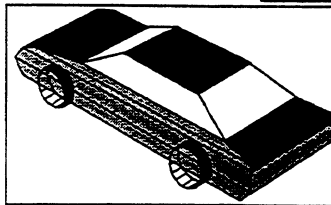
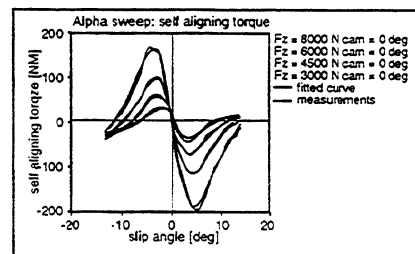
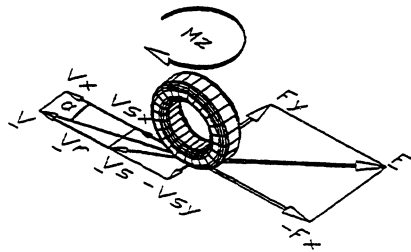
A design and analysis tool, to support testing and modelling of tyre behaviour, to be used with any dynamic system simulation code



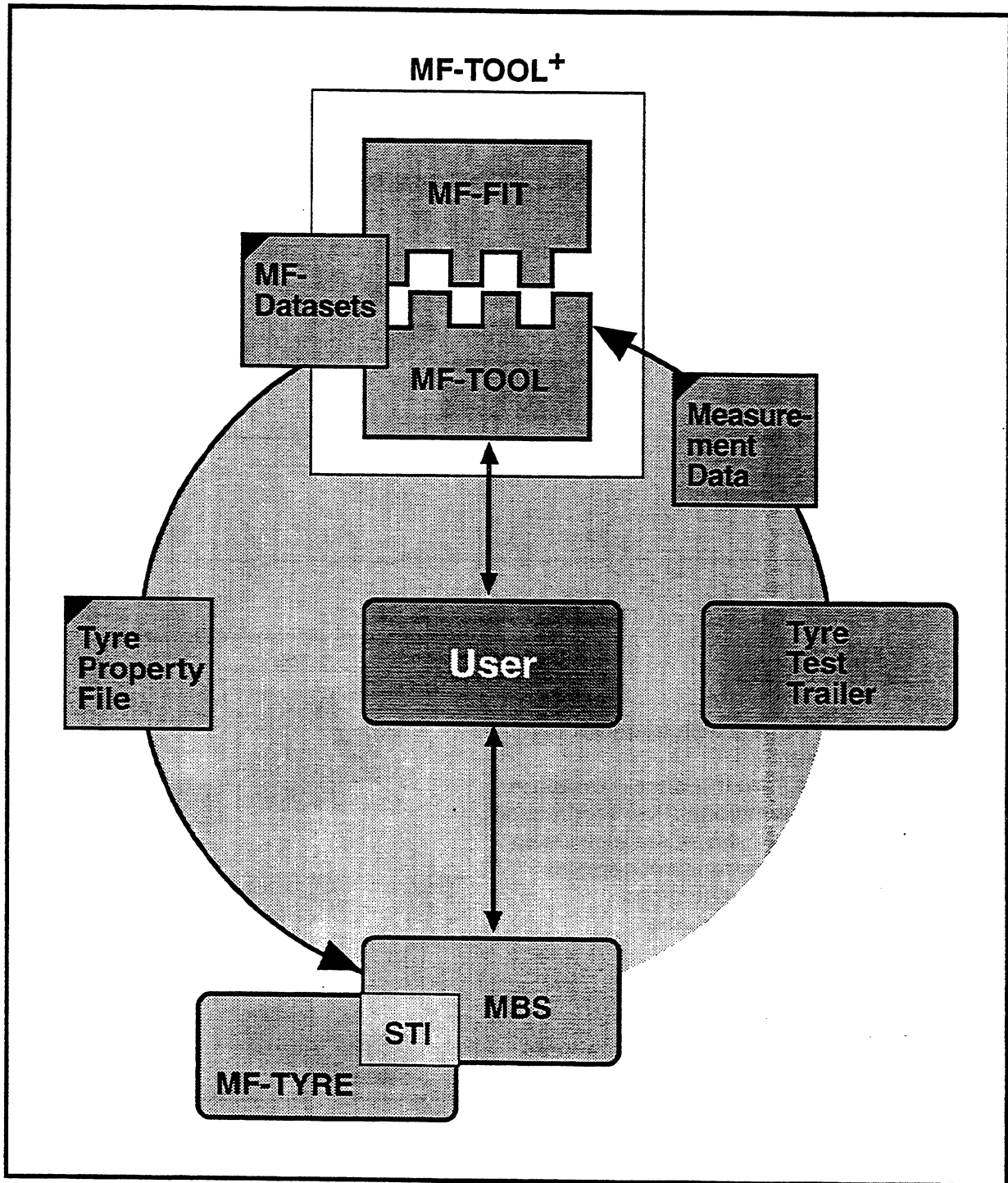
Delft-Tyre a design and analysis tool...



A design and analysis tool, to support testing and modelling of tyre behaviour, to be used with any dynamic system simulation code



Product range



Objectives

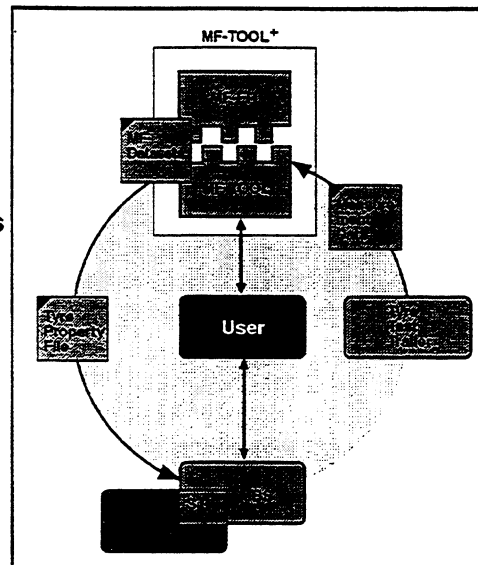
To offer a complete range of tools for modelling and simulation of tyre behaviour

- Tyre model with physical parameters
- Integrated with vehicle simulation environment
- Integrated with tyre data processing
- Tyre characteristic manipulation and tools for tyre-vehicle optimization
- Calculation of tyre model parameters from measurement data
- Latest developments
- Internationally accepted standards
- Open and well-known to the user



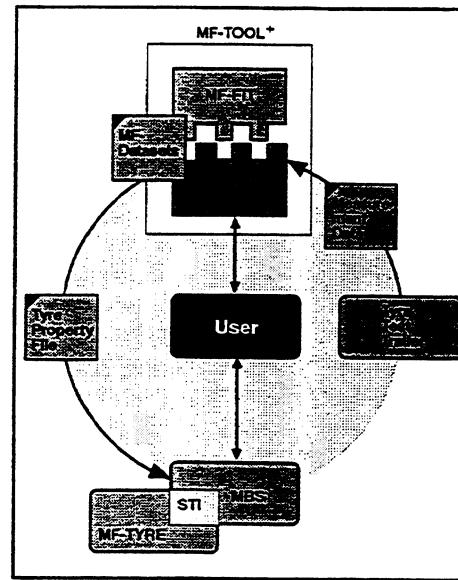
MF-Tyre

- Magic Formula with transient tyre behaviour
- Standard Tyre Interface, developed within International Tyre Workshops
- From simple steady state pure slip conditions to transient complex combined slip situations.
- Real time applications



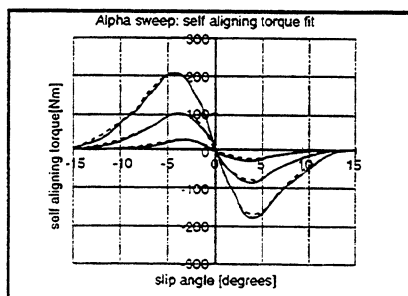
MF-Tool

- Visualisation of tyre characteristics and tyre physical properties
- Adaption and manipulation of tyre characteristics using a graphical interface (user-defined tyre datasets)
- Tyre dataset database
- Preparation of tyre datasets for simulation



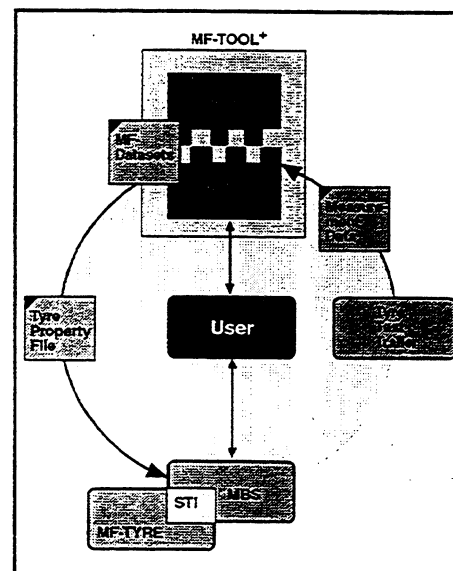
Delft-Tyre

MF-Tool+



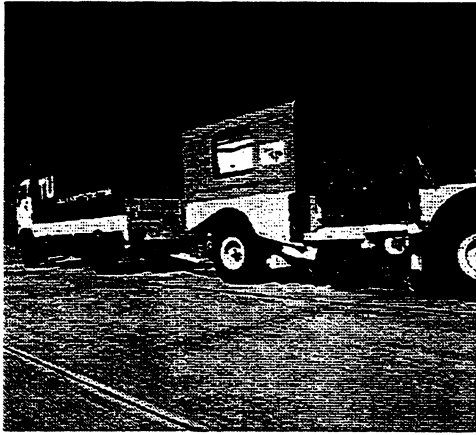
MF-Tool including MF-Fit

- Calculation of tyre model parameters
- Control of MF-Fit
- Graphical comparison measurement data
- Quality check of fit results
- Tyre data in standardized TYDEX format



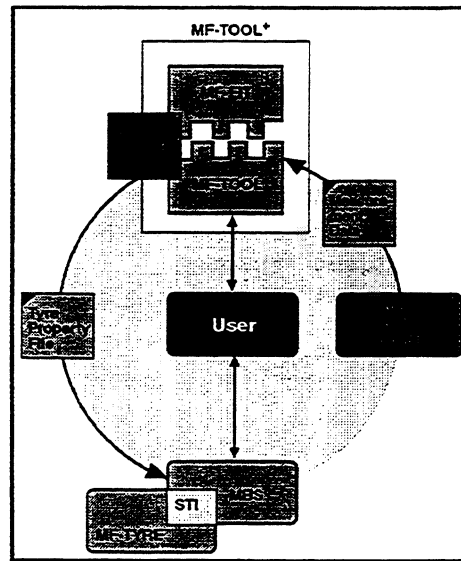
Delft-Tyre

MF-Datasets



- Tyre library
- Regular updates and new datasets
- Tailor made datasets

Delft-Tyre



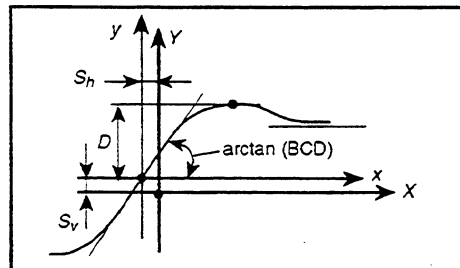
MF-Tyre

- *Steady state:*
MAGIC FORMULA TYRE MODEL

$$y = D \sin [C \arctan \{Bx - E(Bx - \arctan(Bx))\}]$$

$$Y(x) = y(x) + S_v$$

$$x = X + S_h$$



- *Transient and oscillatory aspects:*
FIRST ORDER LAGS and GYROSCOPIC COUPLE

Delft-Tyre

MF-Tyre

MAIN PROPERTIES of NEW VERSION:

Steady state pure slip

- aligning torque based on pneumatic trail

Steady state combined slip

- forces using weighting functions
- aligning torque based on pneumatic trail

Dynamic state

- first order lag
- relaxation lengths in x- and y- directions
- gyroscopic couple about z- axis
- start from zero velocity

Non-dimensional model parameters

Scaling factors



Magic Formula

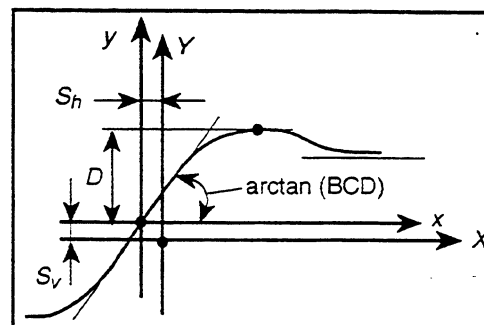
$$y = D \sin [C \arctan \{Bx - E(Bx - \arctan(Bx))\}]$$

$$Y(x) = y(x) + S_v$$

$$x = X + S_h$$

where Y: output variable F_x or F_y
X: input variable α or κ

and B: stiffness factor
C: shape factor
D: peak factor
E: curvature factor
 S_h : horizontal shift
 S_v : vertical shift



Magic Formula / Pure slip

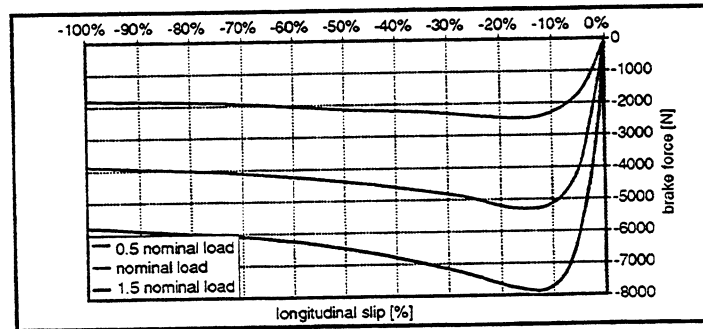
Longitudinal force

$$F_{xo} = D_x \sin [C_x \arctan \{B_x \kappa_x - E_x (B_x \kappa_x - \arctan (B_x \kappa_x))\}] + S_{vx}$$

$$D_x = (p_{Dx1} + p_{Dx2} df_z) F_z \lambda_{\mu x}$$

$$K_x = BCD_x = F_z (p_{Kx1} + p_{Kx2} df_z) \exp(-p_{Kx3} df_z) \lambda_{Kx}$$

etc.



Delft-Tyre

Magic Formula / Pure slip

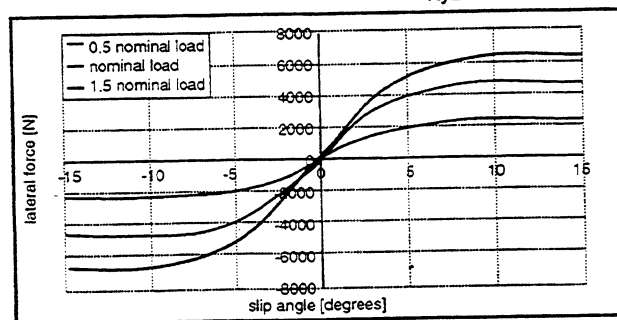
Lateral force

$$F_{yo} = D_y \sin [C_y \arctan \{B_y \alpha_y - E_y (B_y \alpha_y - \arctan (B_y \alpha_y))\}] + S_{vy}$$

$$D_y = (p_{Dy1} + p_{Dy2} df_z) F_z \lambda_{\mu y}$$

$$K_y = BCD_y = p_{Ky1} F_{zo} \sin [2 \arctan \{ \frac{F_z}{p_{Ky2} F_{zo} \lambda_{Fzo}} \}] (1 - p_{Ky3} |\gamma_y|) \lambda_{Fzo} \lambda_{Ky}$$

etc.



Delft-Tyre

Magic Formula

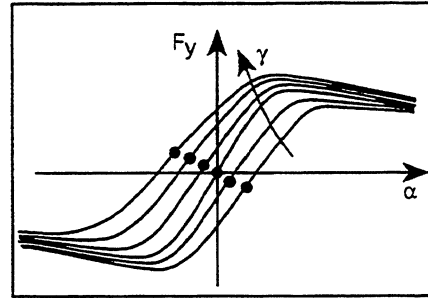
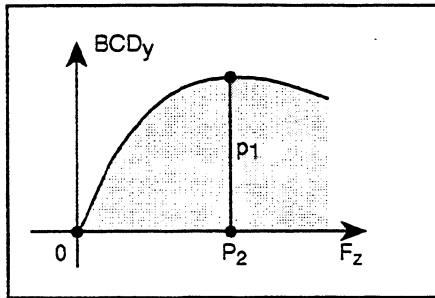
Pure slip

Asymmetry

Curvature factor E
Cornering stiffness

$$E = E_0 + \Delta E \operatorname{sign}(x)$$

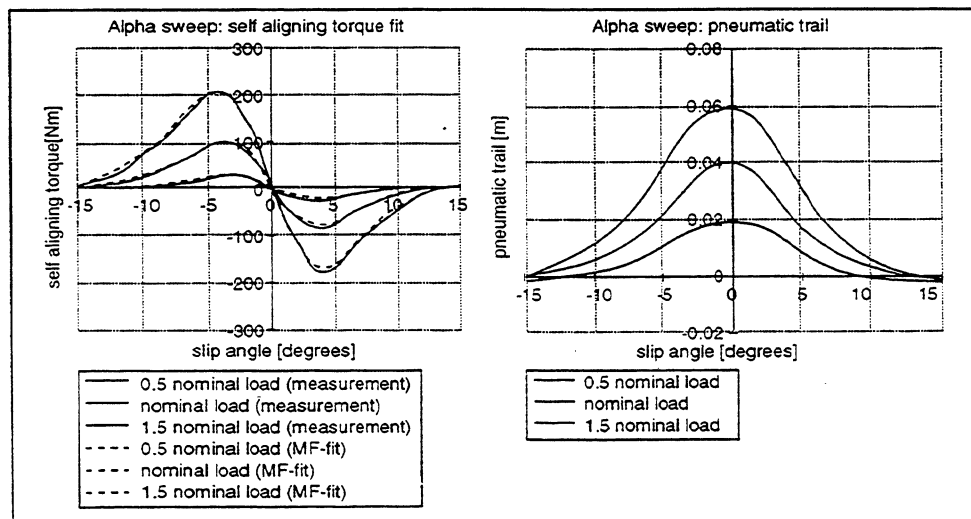
$$BCD_y = p_1 \sin \left[2 \arctan \left(\frac{F_z}{p_2} \right) \right] (1 - p_3 |\gamma|)$$



Delft-Tyre

Magic Formula

Aligning torque



Delft-Tyre

Magic Formula / Pure slip

Aligning torque

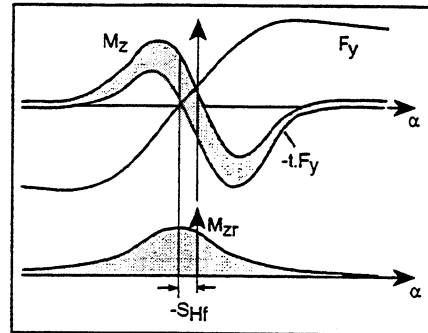
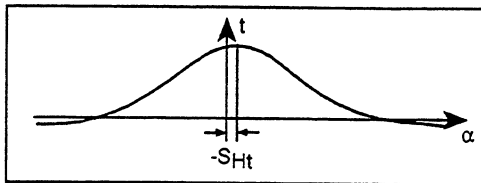
$$M_{zo} = -t F_{y0} + M_{zr}$$

Pneumatic trail

$$t(\alpha_r) = D_t \cos [C_t \arctan \{B_t \alpha_r - E_t (B_t \alpha_r - \arctan (B_t \alpha_r))\}] ; \alpha_r = \alpha + S_{Ht}$$

Residual torque

$$M_{zr}(\alpha_r) = D_r \cos [\arctan (B_r \alpha_r)] ; \alpha_r = \alpha + S_{Hr}$$



Delft-Tyre

Magic Formula / Combined slip

Weighting functions G multiplied with pure slip functions

Weighting function have a hill shape

Cosine version of Magic Formula is used

$$G = D \cos [C \arctan (Bx)]$$

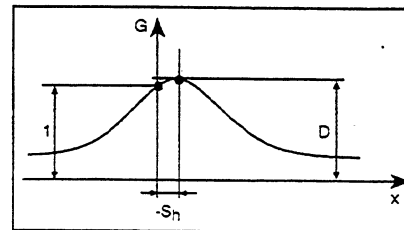
x is either κ or α (possibly shifted)

D represents the peak value

C determines the height of the hill's base

B influences the sharpness of the hill

E is not needed to improve the fit



Delft-Tyre

Magic Formula

Combined slip

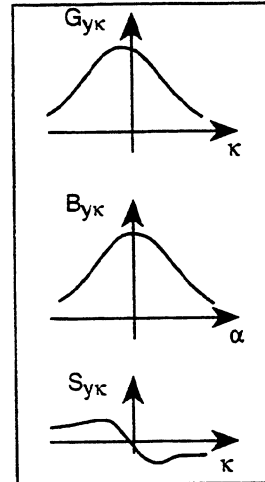
Side force

$$F_y = G_{y\kappa} F_{y0} + S_{vy\kappa}$$

$$G_{y\kappa} = \frac{\cos[C_{y\kappa} \arctan\{B_{y\kappa}(\kappa + S_{Hy\kappa})\}]}{\cos[C_{y\kappa} \arctan(B_{y\kappa} S_{Hy\kappa})]}$$

$$B_{y\kappa} = r_{By1} \cos [\arctan \{r_{By2}(\alpha - r_{By3})\}]$$

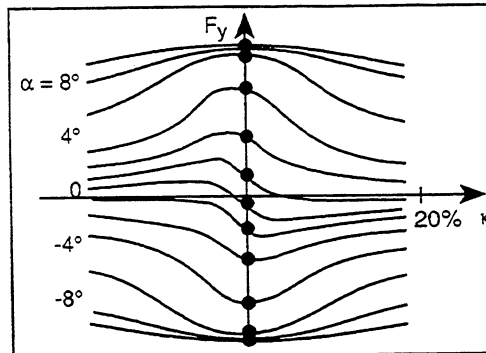
$$S_{vy\kappa} = \sin [r_{vy5} \arctan (r_{vy6} \kappa)]$$



Magic Formula

Combined slip

- F_{y0} is the side force at pure side slip
- $B_{y\kappa}$ influences the sharpness of the hill
- $S_{vy\kappa}$ is the vertical shift due to ' κ -induced' plysteer.



Magic Formula

Combined slip

Longitudinal force

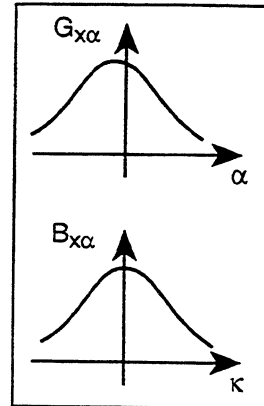
$$F_x = G_{x\alpha} F_{xo}$$

$$G_{x\alpha} = \frac{\cos[C_{x\alpha} \arctan\{B_{x\alpha}(\alpha + S_{Hx\alpha})\}]}{\cos[C_{x\alpha} \arctan(B_{x\alpha} S_{Hx\alpha})]}$$

$$C_{x\alpha} = r_{Cx1}$$

$$B_{x\alpha} = r_{Bx1} \cos [\arctan \{r_{Bx2} \kappa\}]$$

$$S_{Hx\alpha} = r_{Hx1}$$

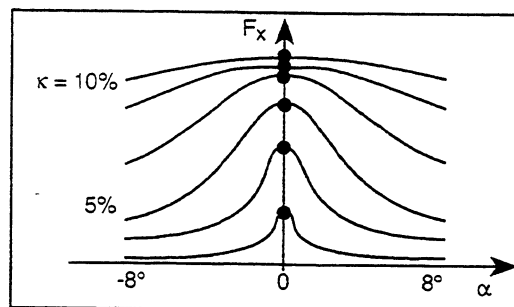


Delft-Tyre

Magic Formula

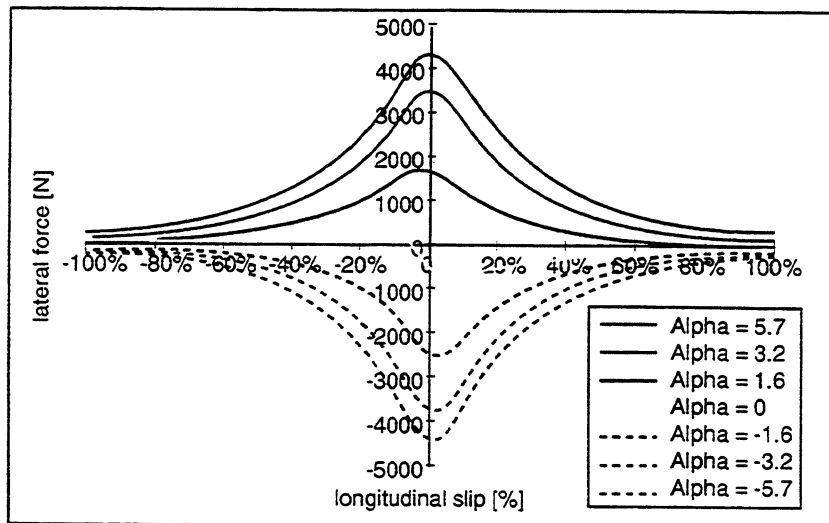
Combined slip

- F_{xo} is the longitudinal force at pure longitudinal slip
- $B_{x\alpha}$ influences the sharpness of the hill
- $C_{x\alpha}$ influences the height of the hill base
- $S_{Hx\alpha}$ is the horizontal shift of the hill peak



Delft-Tyre

Magic Formula



Magic Formula

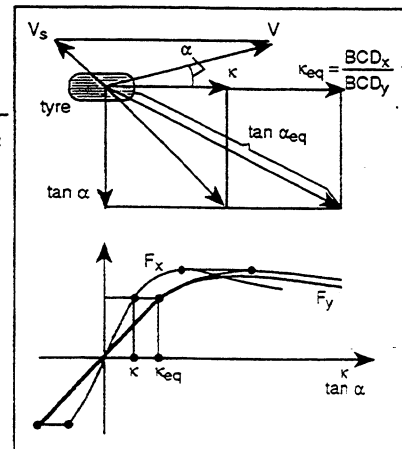
Combined slip

Aligning torque

$$M_z = -t(\alpha_{t,eq}) F_y + M_z(\alpha_{t,eq}) + s(F_y \gamma) F_x$$

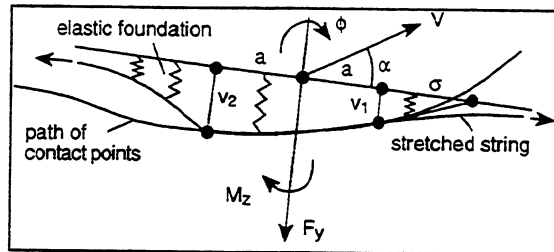
$$\alpha_{t,eq} = \text{sign}(\alpha_{t,r}) \cdot \arctan \sqrt{\tan^2(\alpha_{t,r}) + \left(\frac{BCD_x}{BCD_y}\right)^2 \kappa^2}$$

$$s = \{s_{sz1} + s_{sz2} \left(\frac{F_y}{F_{zo}}\right) + (s_{sz3} + s_{sz4} df_z) \gamma\} R_o \lambda_s$$



Transient aspects

$$\frac{1}{V_x} \frac{dv_1}{dt} + \frac{v_1}{\sigma} = \tan(\alpha) - a\phi$$



Multiplication by V_x and σ , neglect turn slip ϕ

$$\sigma \frac{dv_1}{dt} + V_x v_1 = -\sigma V_{sy}$$

NOW POSSIBLE TO START AND STOP!

deflection angle α' $\tan(\alpha') = \frac{v_1}{\sigma}$



Dynamic Combined Slip

- slip speeds $V_{sx,y}$ input instead of κ and α
- longitudinal and lateral deformations u and v
- relaxation lengths σ_κ and σ_α
- speed of rolling V_r

$$\sigma_\kappa \frac{du}{dt} + |V_r| u = -\sigma_\kappa V_{sx} \quad \sigma_\alpha \frac{dv}{dt} + |V_r| v = -\sigma_\alpha V_{sy}$$

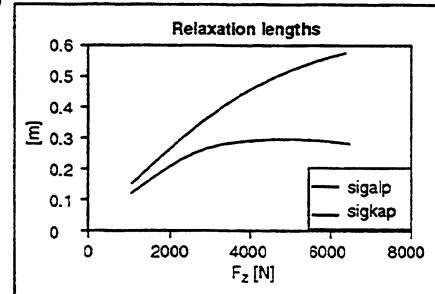


Dynamic Combined Slip

Relaxation lengths depend on vertical load and camber:

$$\sigma_{\kappa} = F_z (p_{Tx1} + p_{Tx2} df_z) \exp(-p_{Tx3} df_z) (R_0/F_{z0}) \lambda_{\sigma\kappa}$$

$$\sigma_{\alpha} = p_{Ty1} \sin [2 \arctan \{ \frac{F_z}{p_{Ty2} F_{z0} \lambda_{Fz0}} \}] (1 - p_{Ky3} | \gamma |) R_0 \lambda_{Fz0} \lambda_{\sigma\alpha}$$



Dynamic Combined Slip

Theoretical tyre deformation slip components:

$$\zeta'_x = \frac{u}{\sigma_x}, \quad \zeta'_y = \frac{v}{\sigma_{\alpha}}$$

and the practical tyre deformation slip quantities:

$$\kappa' = \frac{\zeta'_x}{\text{sign } V_r - \zeta'_x}, \quad \tan(\alpha') = \frac{\zeta'_y}{\text{sign } V_r - \zeta'_x}$$

Forces and moment (steady state formulae)

$$F_x = F_x(\alpha', \kappa', F_z)$$

$$F_y = F_y(\alpha', \kappa', \gamma, F_z)$$

$$M'_z = M'_z(\alpha', \kappa', \gamma, F_z)$$



Gyroscopic Couple

Moment due to tyre inertia acting about the z-axis

$$M_{z,gyr} = C_{gyr} m_t V_r \frac{dv}{dt}$$

Total aligning torque

$$M_z = M_z' + M_{z,gyr}$$



Scaling factors

Pure slip

λ_{Fz0}	nominal load
$\lambda_{\mu x}, \lambda_{\mu y}$	peak friction levels F_x, F_y
$\lambda_{Kx}, \lambda_{Ky}$	slip stiffness
$\lambda_{\gamma y}$	camber force stiffness
$\lambda_{\gamma z}$	camber torque stiffness
λ_t	pneumatic trail
λ_{Mr}	residual torque



Scaling factors

Combined slip

$\lambda_{x\alpha}$	α influence on F_x (κ)
$\lambda_{y\kappa}$	κ influence on $F_y(\alpha)$
$\lambda_{vy\kappa}$	κ induced F_y
λ_s	M_z moment arm of F_x

Transient response

$\lambda_{\sigma\kappa}$	relaxation length for F_x
$\lambda_{\sigma\alpha}$	relaxation length for F_y
λ_{gyr}	tyre mass (gyroscopic couple)



TYDEX Workshops

International group of vehicle and tyre manufacturers
with the objective to standardize interfaces between

vehicle models - tyre models - tyre data

- **Standard Tyre Interface (STI)**
Interface between vehicle model and any tyre model
to enable simple exchange of tyre models
- **TYDEX data format**
Format for simple exchange of tyre test data and
parameters of tyre models
- **International Colloquia on Tyre Modelling**



MF-Datasets

Library

Contents (Jan. 1996)

tyre	manufacturer	type	conditions
175/70 R13	Michelin	MXT	dry
195/65 R15	Michelin	MXV3a Energy	dry
195/65 R15	Michelin	Pilot HX MXV3a	dry, wet
195/65 R15	Vredestein	Snowtrac	dry
225/50 R16	Goodyear	Eagle GST	dry, wet
235/75 R15	Goodyear	Invicta GS	dry, wet



MF-Datasets

Tyre datasets

Steady state:

- Pure and combined slip
- Effective tyre radius
- Vertical tyre stiffness

Dynamic:

- Tire lags depending on load

