
Semi-physical Tire Model for Cornering Simulations of Vehicles

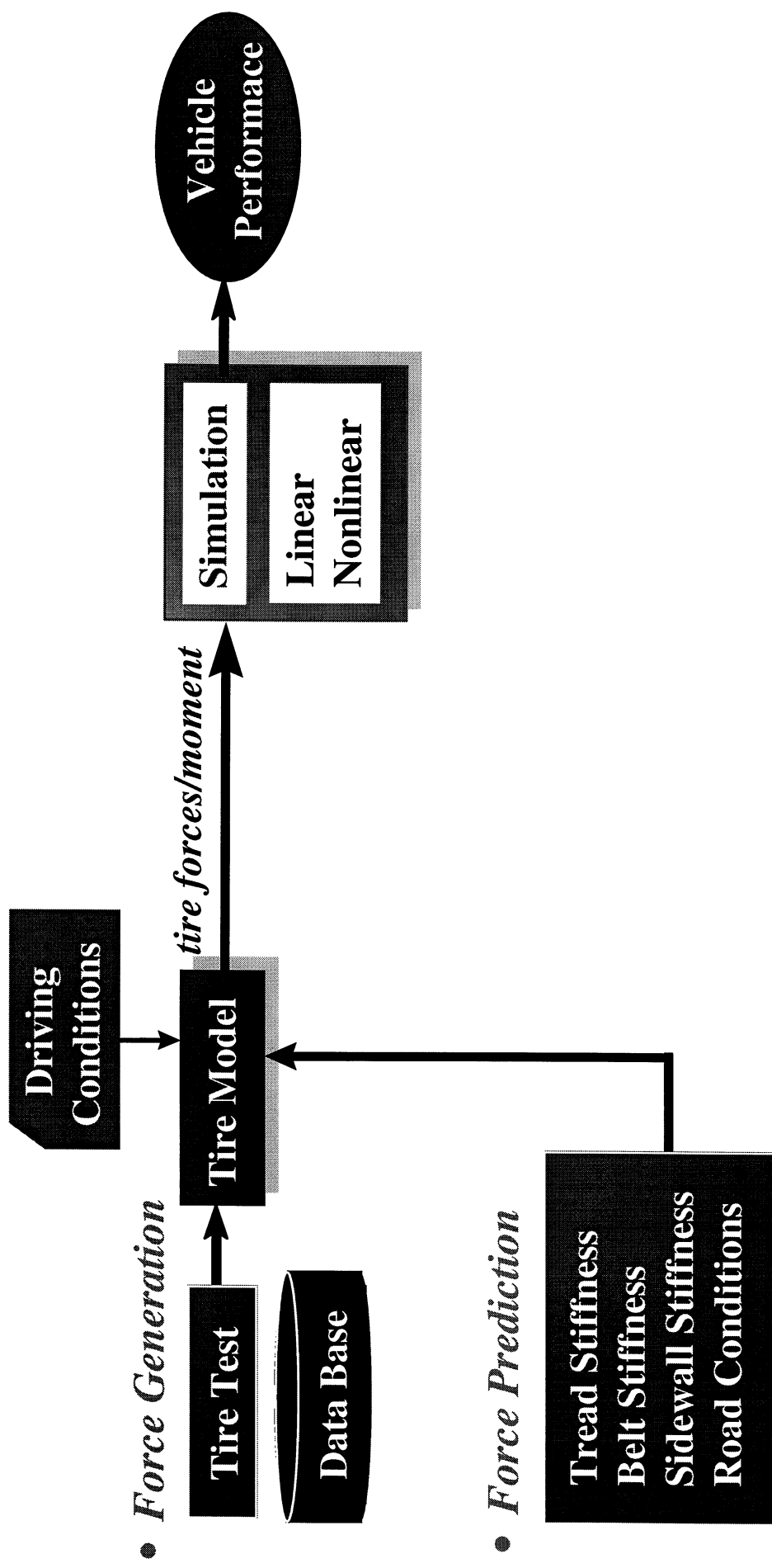
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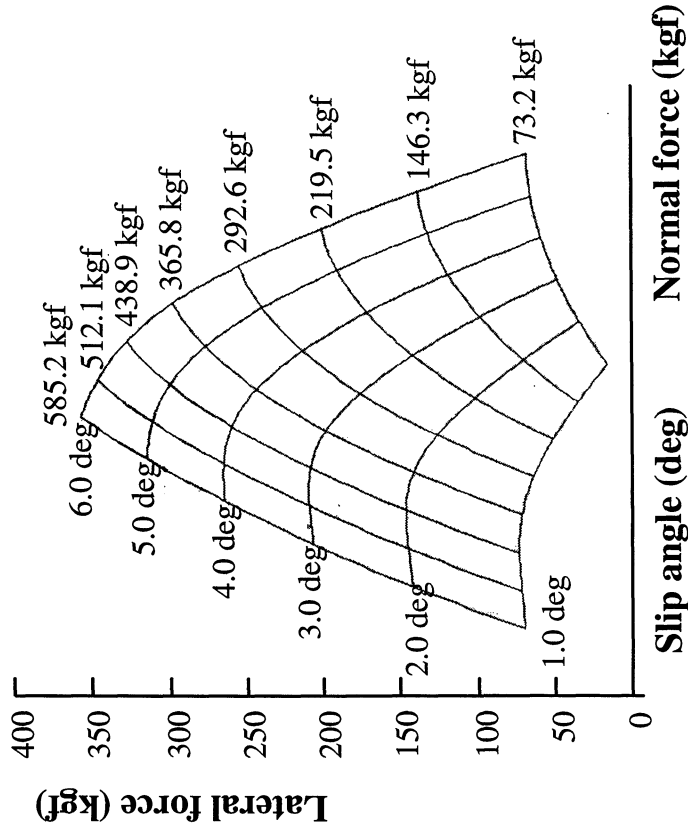
Contents

- **Role of Tire Model in Tire Design Process**
- **Motivation and Objective of This Study**
- **Empirical Considerations**
- **Longitudinal Force at Pure Slip**
- **Lateral Force and Moment at Pure Slip**
- **Forces/Moment at Combined Slip**
- **Forces/Moment at Transient**
- **Conclusios**

Role of Tire Model in Tire Design Process



Using the Raw Data



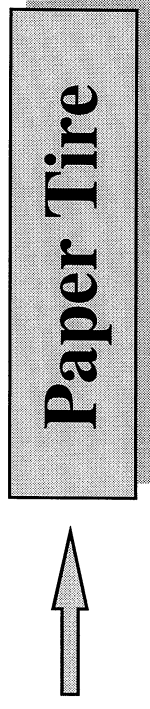
- Carpet plot
- Interpolation
- Exact value at measured points
- A lot of time and cost for experiment
- Can not get the data beyond experiment
- Hard to get convergence in Simulation

Previous Tire Model

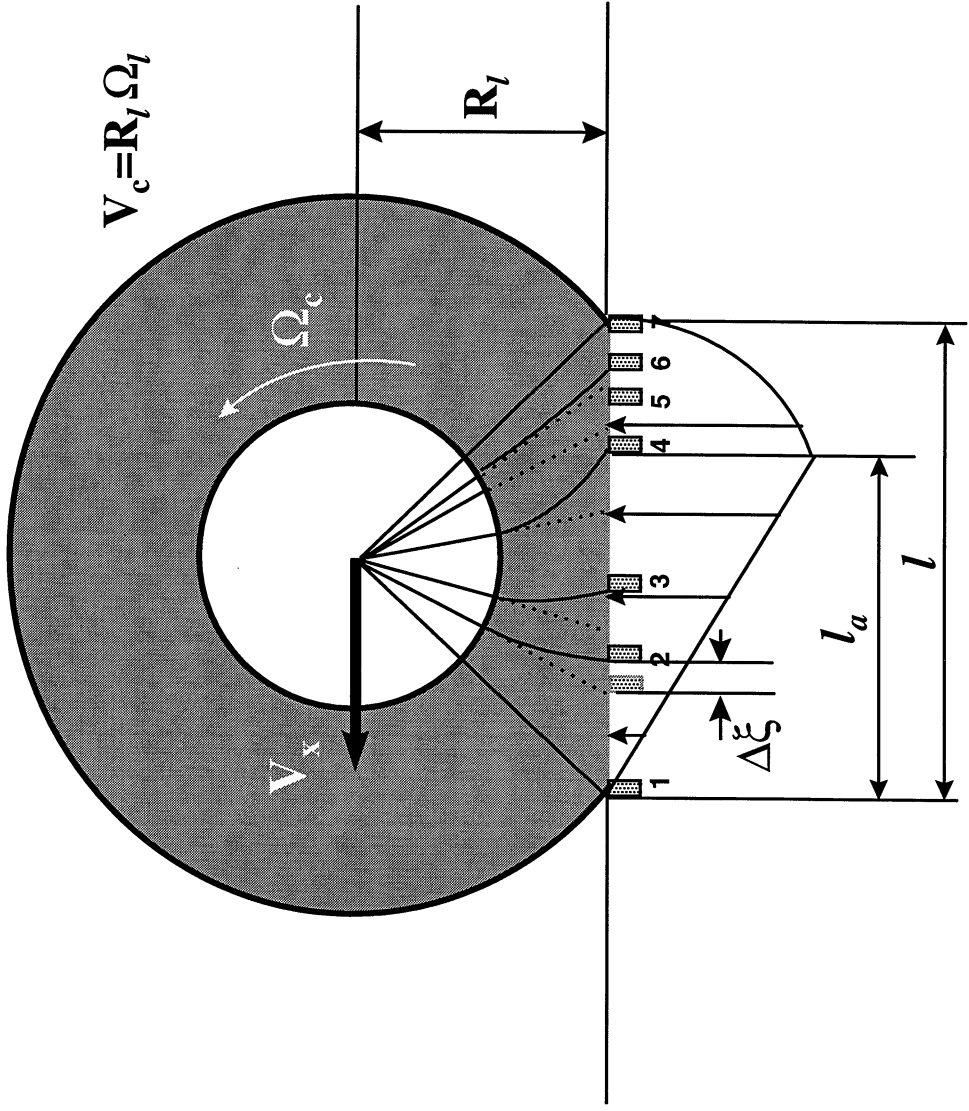
- **Analytical model**
 - Sakai model, UA-tire model
 - Based on physical concept
 - Small number of parameters
 - Not enough for practical simulations
- **Empirical model**
 - Magic formula, Polynomial model
 - Curve fitting the measured data using specific functions
 - More accurate than analytical models
 - Hard to use without experimental data

New Semi-physical Model

- Analytical + empirical model
- Accurate tire forces/moment
 - For various driving conditions
 - slip ratio, slip angle, camber angle and load
 - Transient
- Based on physical concept
 - Tire component stiffness and pneumatic trail
 - Fewer parameters than empirical models
 - Provision of possibility that a designer can predict tire forces/moment for modified tire design



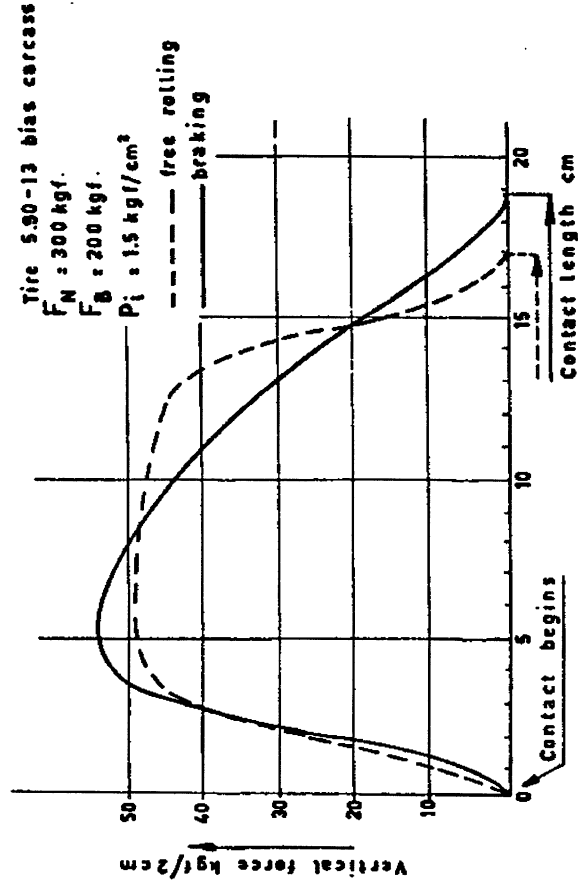
Generation of the Longitudinal Force



$$F_{\xi} = \int_0^w \int_0^{l_a} \sigma_{\xi}^{(a)} d\xi d\eta + \int_0^w \int_{l_a}^l \sigma_{\xi}^{(s)} d\xi d\eta$$

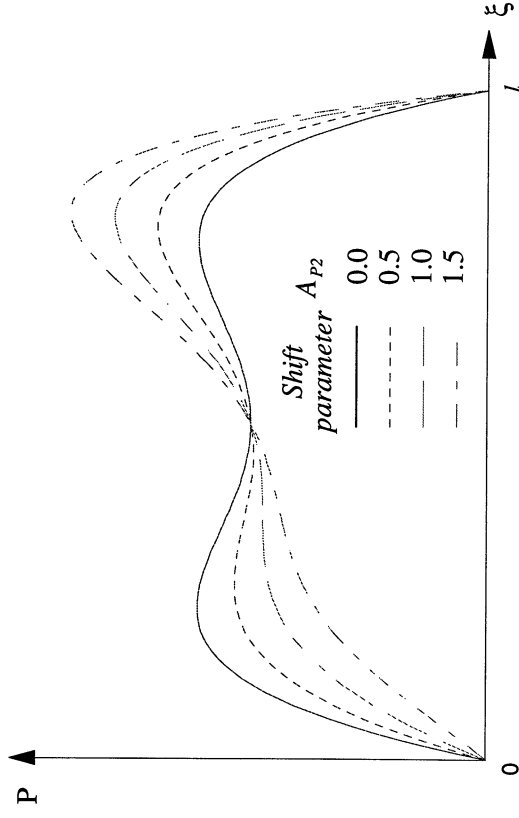
Contact Pressure Distribution

Contact pressure distribution for free rolling and braking



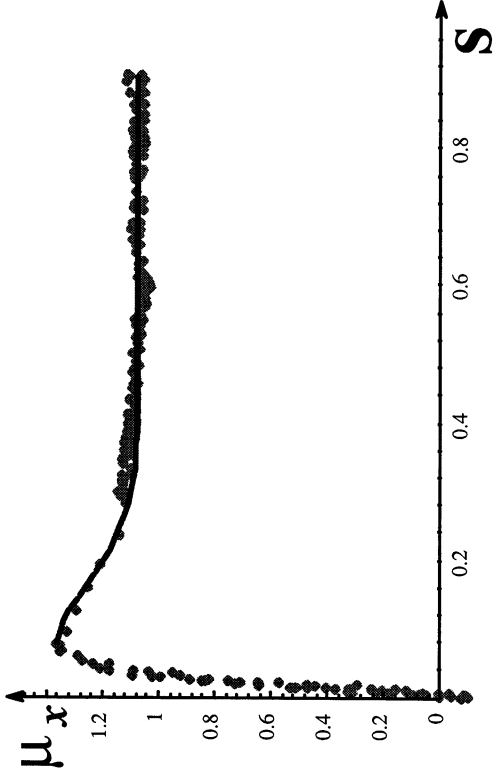
Generated by function

$$P = \frac{120F_z}{(20 + A_{p1}) \cdot w \cdot l} \cdot \frac{\xi}{l} \cdot \left(1 - \frac{\xi}{l}\right) \cdot \left[1 + A_{p1} \left(\frac{\xi}{l} - \frac{1}{2}\right)^2\right] \cdot \left[1 + A_{p2} \left(\frac{\xi}{l} - \frac{1}{2}\right)\right]$$



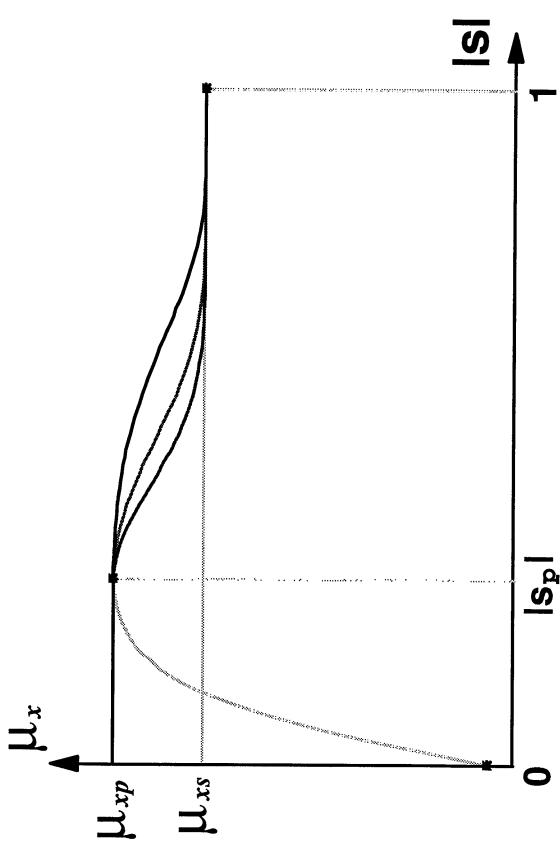
Friction Coefficient

Longitudinal friction force



Generated by function

$$\mu_x = \mu_{xs} + (\mu_{xp} - \mu_{xs}) \operatorname{sech} \left(A_{\mu s1} \tanh \left(A_{\mu s2} (|s| - |s_p|) \right) \right) / (1 - |s|)$$



Adhesive Contact Length

$$l_n(s) = \text{sech} \left[a \tanh(b |s|) / (1 - |s|) \right]$$

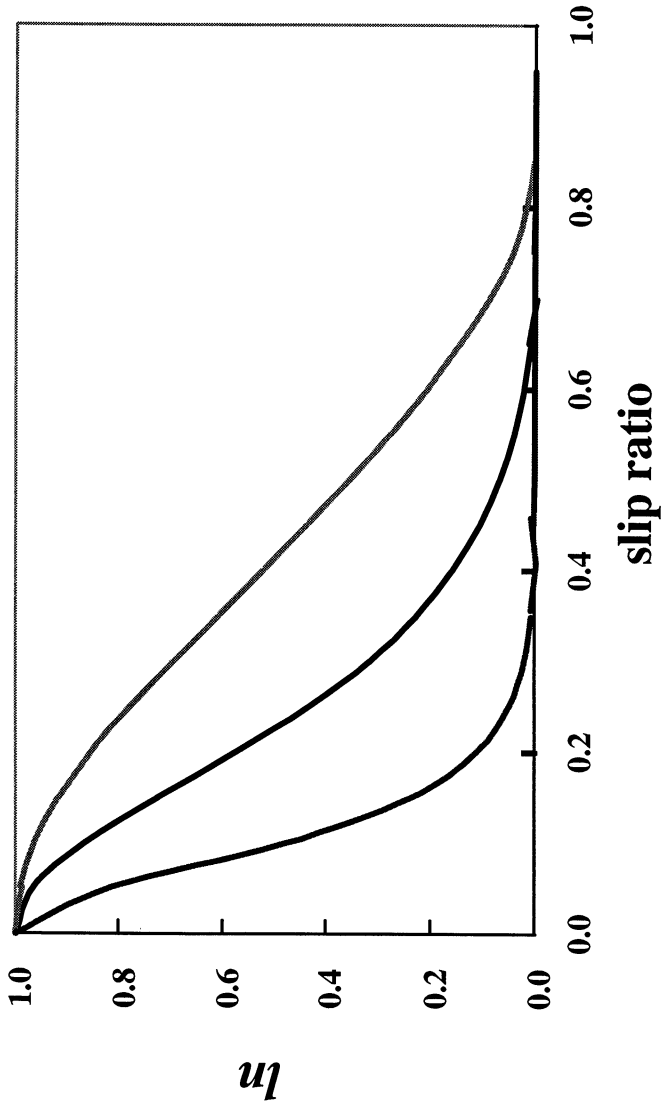
$$l_n = \frac{\text{adhesive length}}{\text{contact length}}$$

B.C

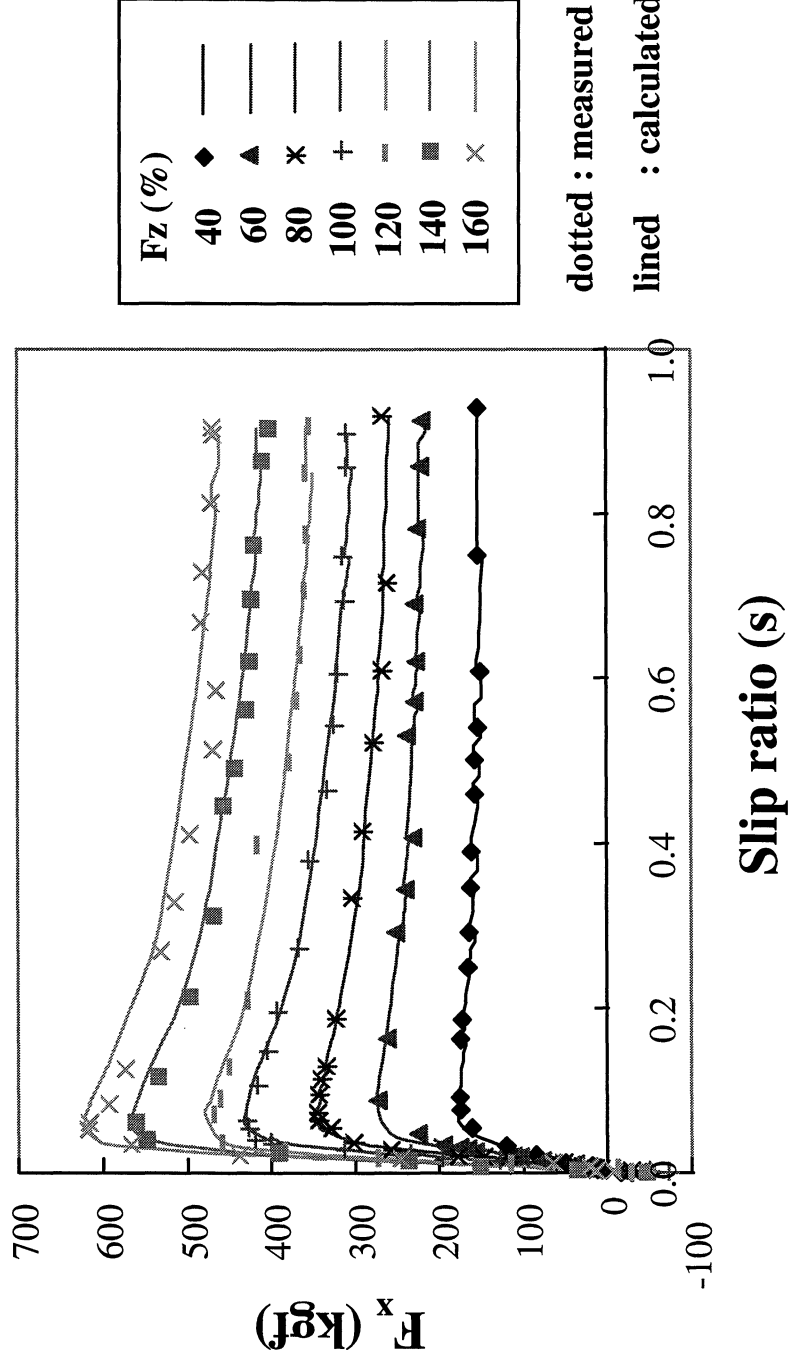
$$l_n \Big|_{s=0} = 1$$

$$l_n \Big|_{s=1} = 0$$

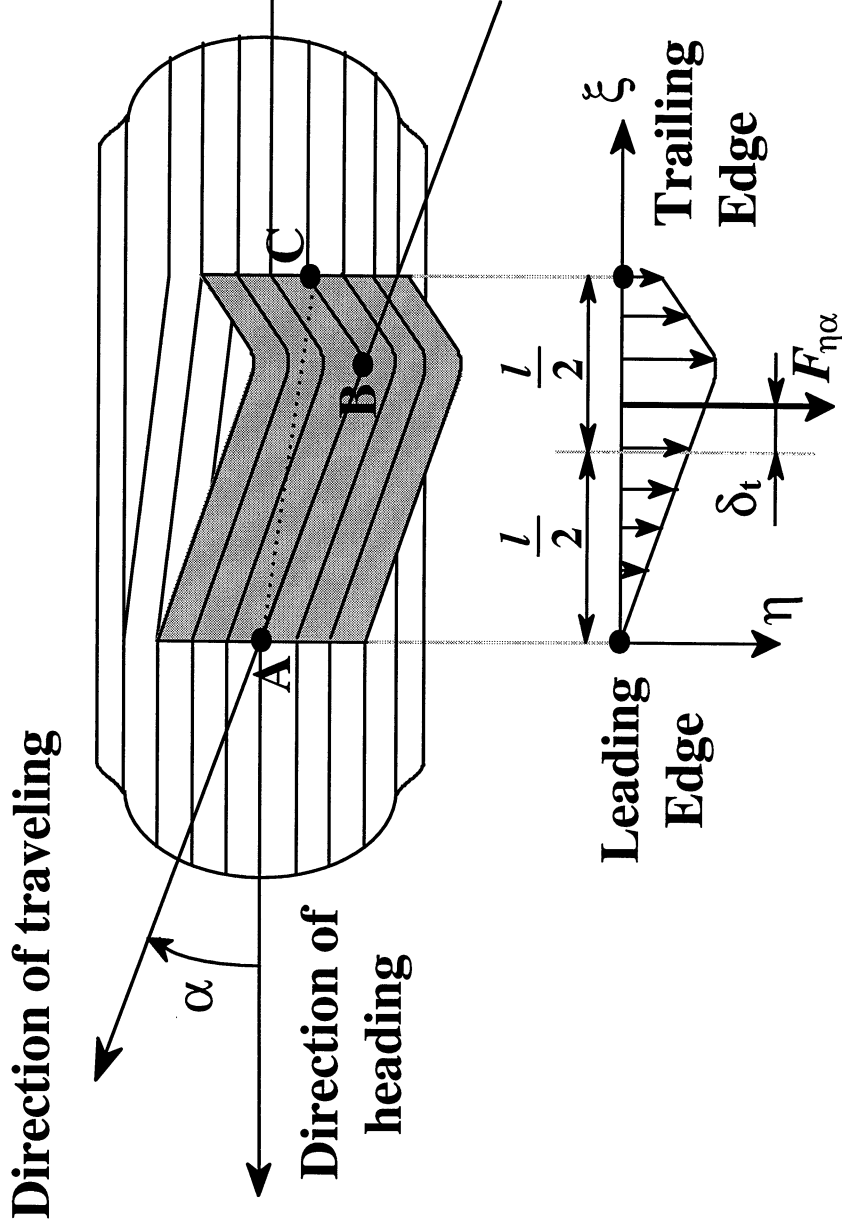
$$l_n \approx 1 \text{ for } s \ll 1$$



Longitudinal Force for various Loads



Generation of the Lateral Force

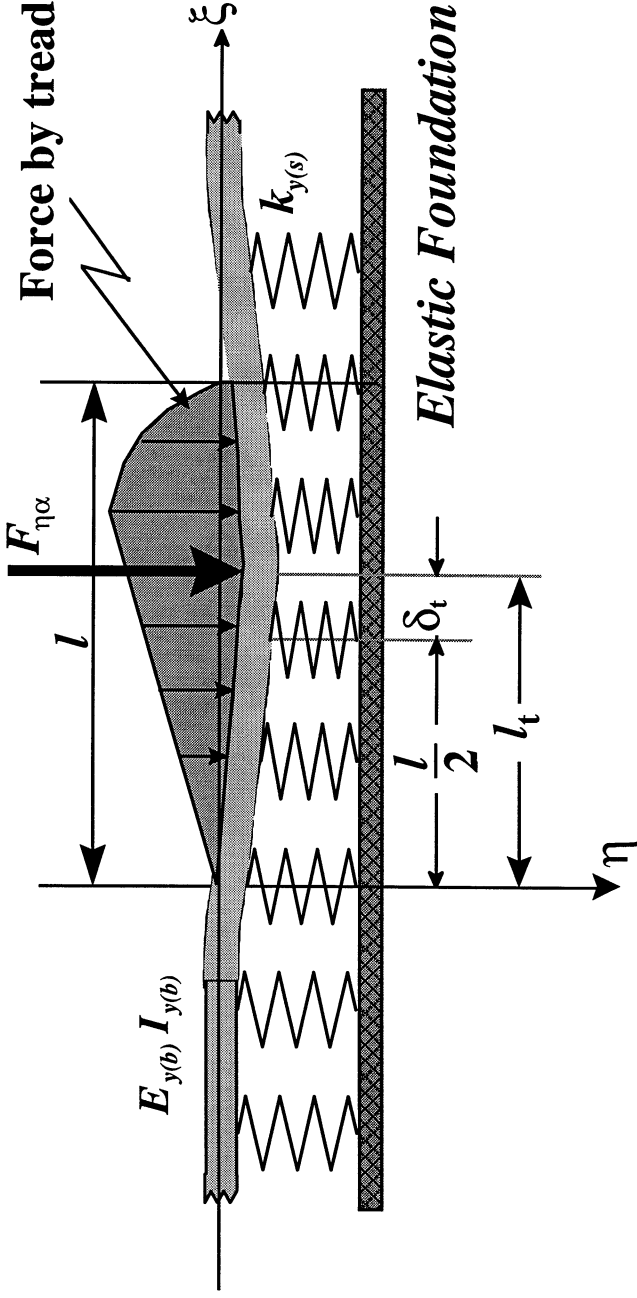


Elastic Founded Beam Model

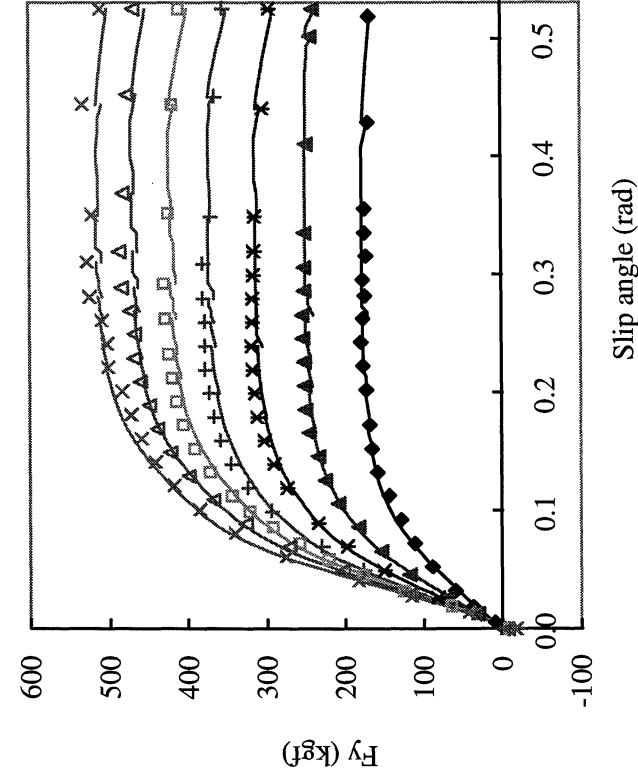
$$E_{y^{(b)}} I_{y^{(b)}} \frac{d^4 \eta}{d\xi^4} + k_{y^{(s)}} \eta = F_{\eta\alpha} \cdot \delta(\xi - l_t)$$

$$F_\eta = \int_0^w \int_0^{l_a} \sigma_{\eta\alpha}^{(a)} d\xi dw + \int_0^w \int_0^{l_a} \sigma_{\eta\alpha}^{(s)} d\xi dw$$

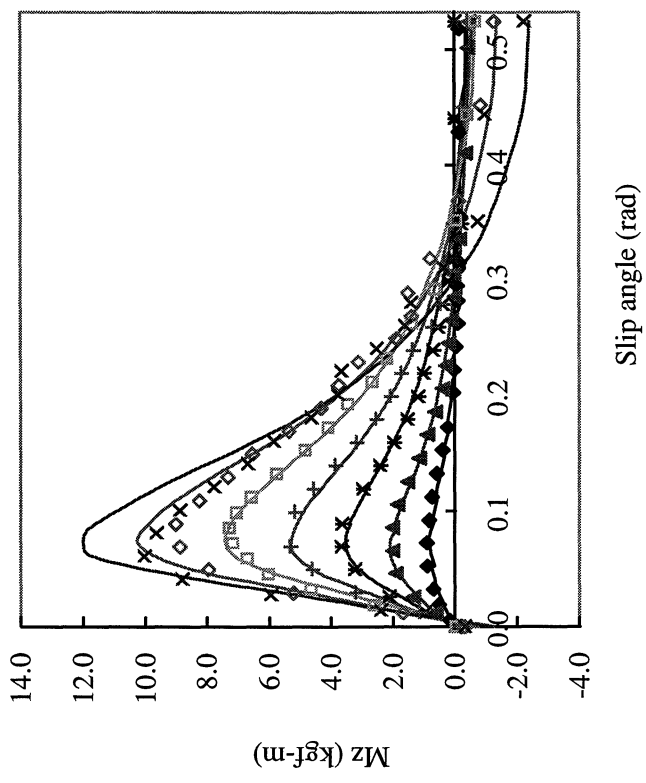
$$M_{z\alpha} = \int_0^w \int_0^{l_a} (\xi - l/2) \sigma_{\eta\alpha}^{(a)} d\xi dw + \int_0^w \int_0^{l_a} (\xi - l/2) \sigma_{\eta\alpha}^{(s)} d\xi dw$$



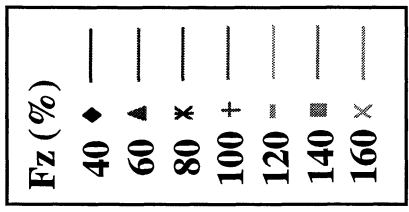
Lateral force/moment for Various Loads



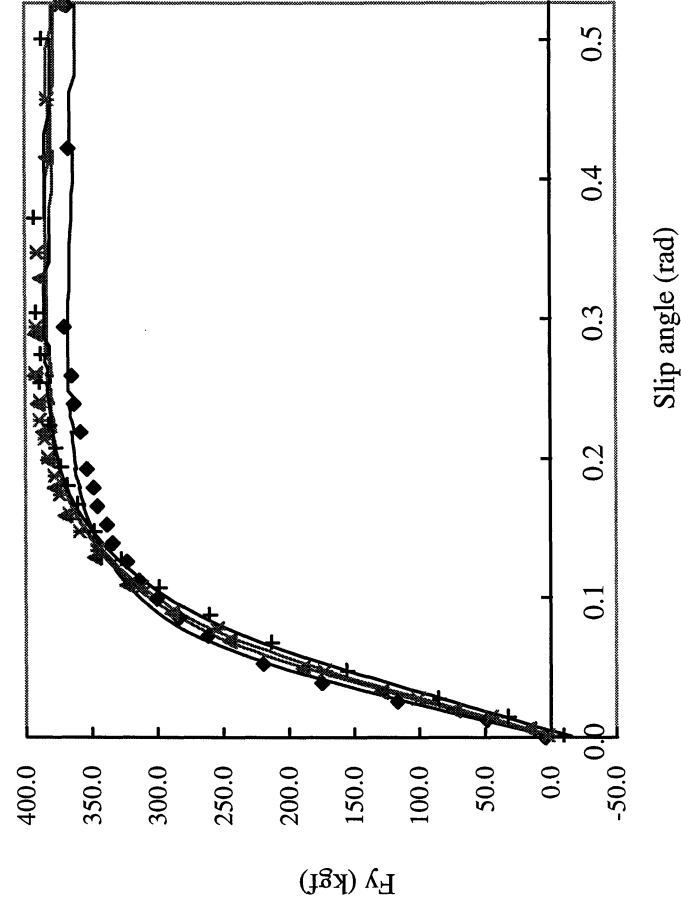
Lateral Force



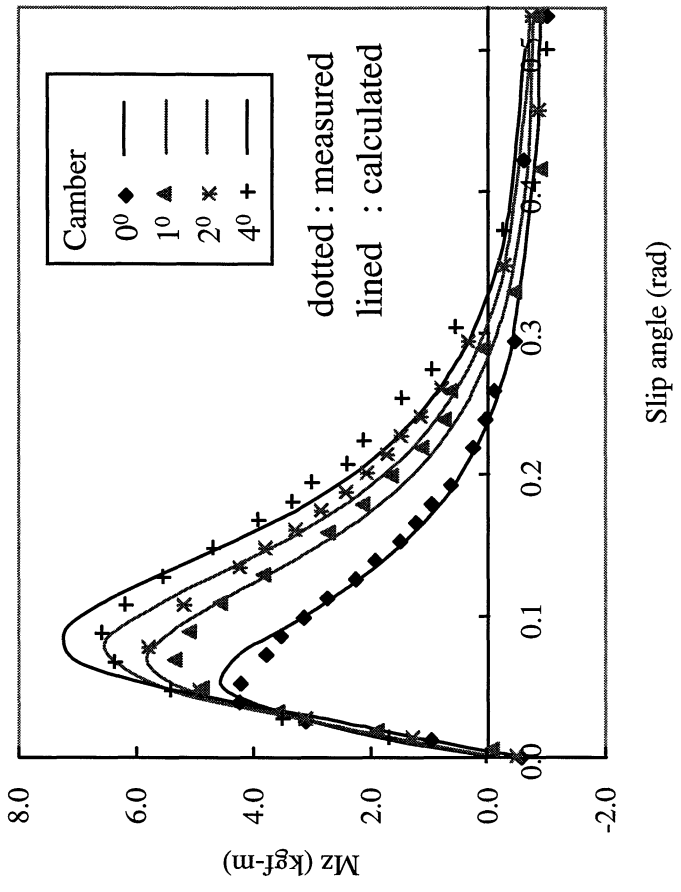
Self-aligning moment



Lateral Force/moment for Camber Angle

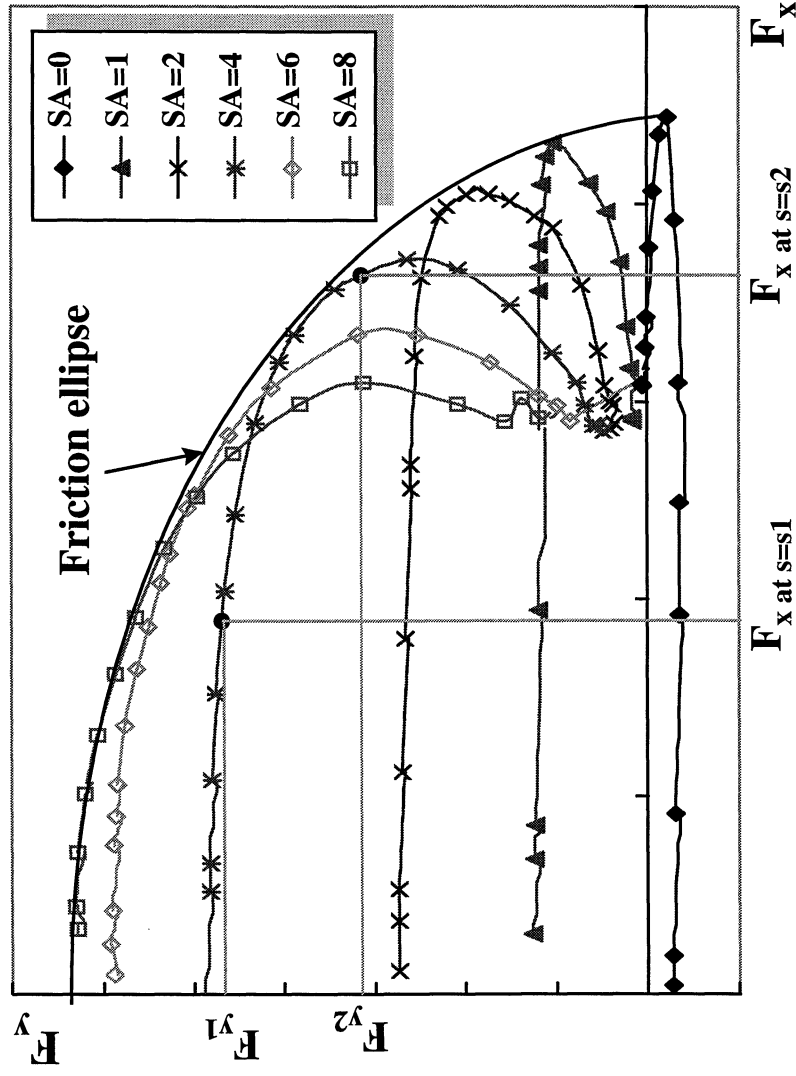


Lateral Force

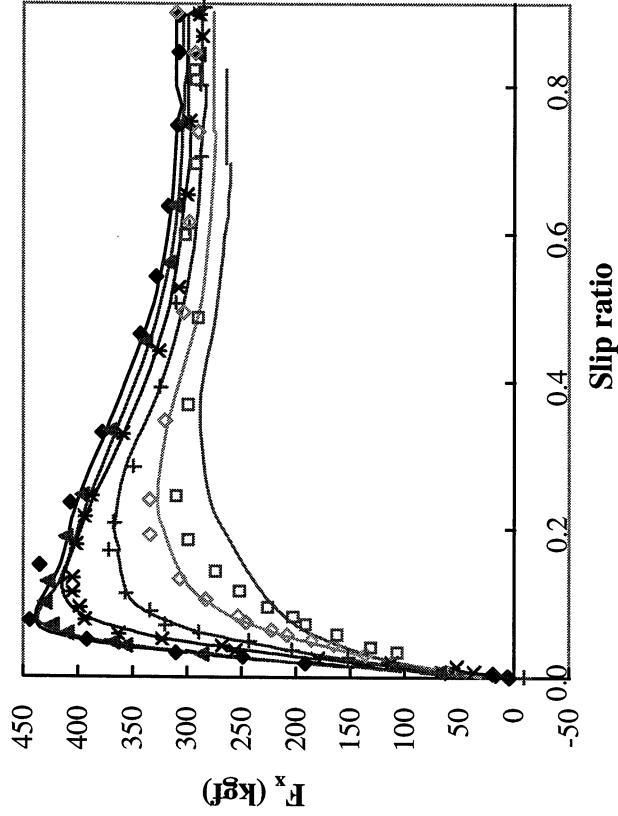


Self-aligning moment

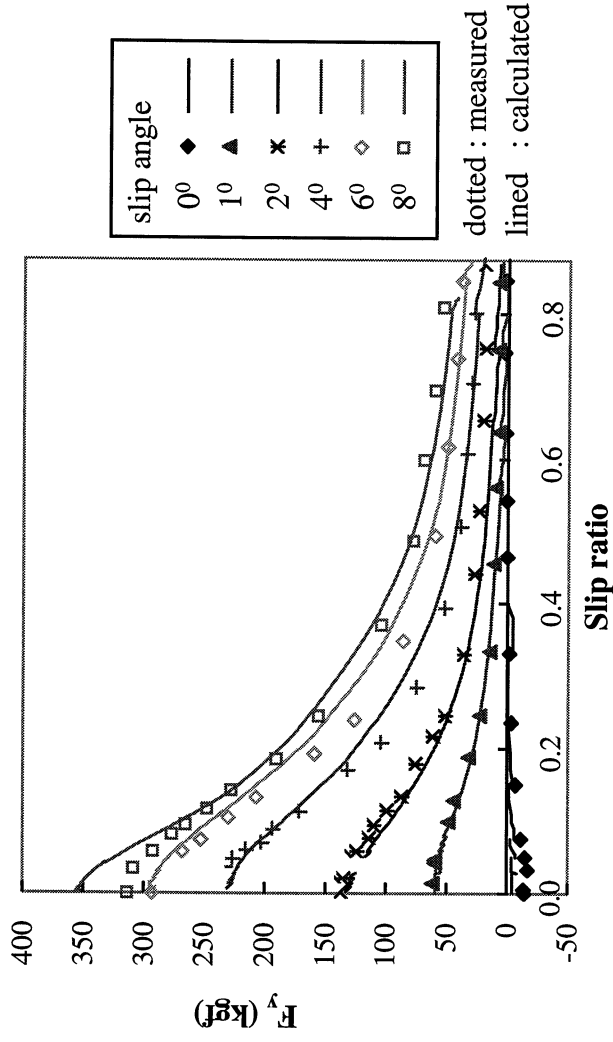
Longitudinal/Lateral Forces at Combined Slip



Longitudinal/Lateral Forces at Combined Slip

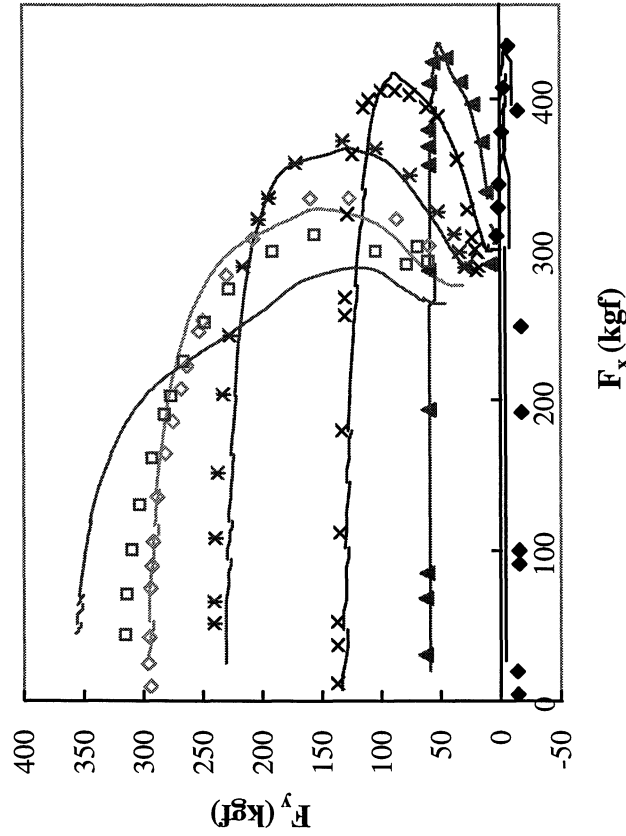


F_x vs. slip ratio for various slip angle

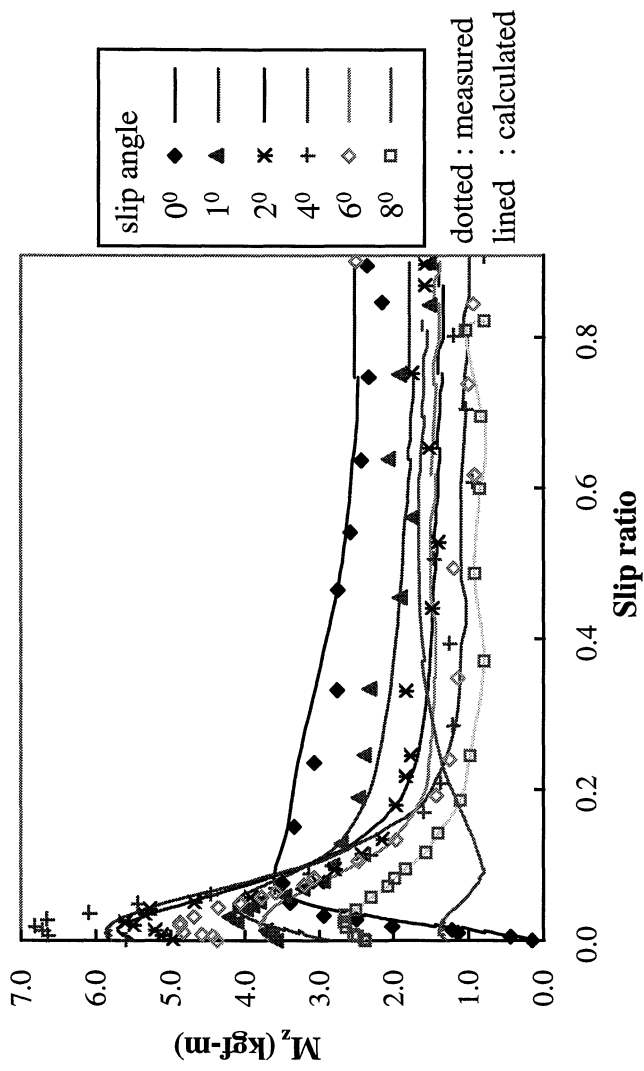


F_y vs. slip ratio for various slip angle

Forces/moment at Combined Slip



F_y vs. F_x for various slip angle

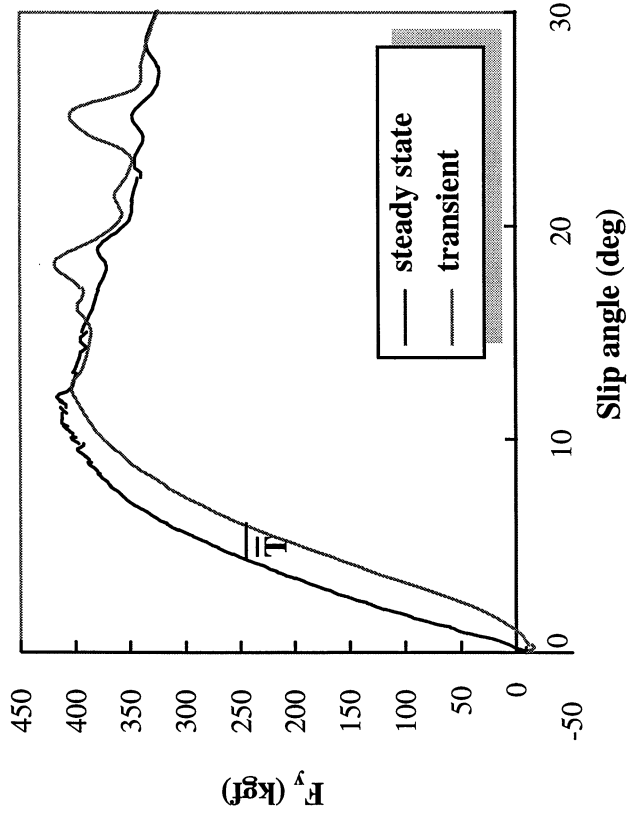


M_z vs. slip ratio for various slip angle

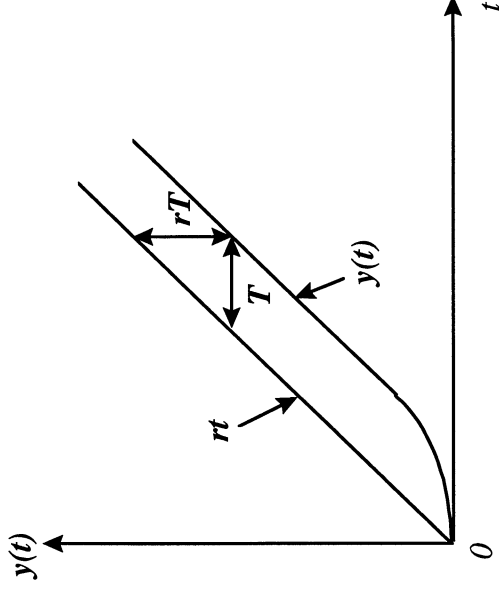
Transient Characteristics of Tire

$$T \frac{dy(t)}{dt} + y(t) = f(t)$$

$$y(t) = r(t - T) + Te^{-t/T}$$

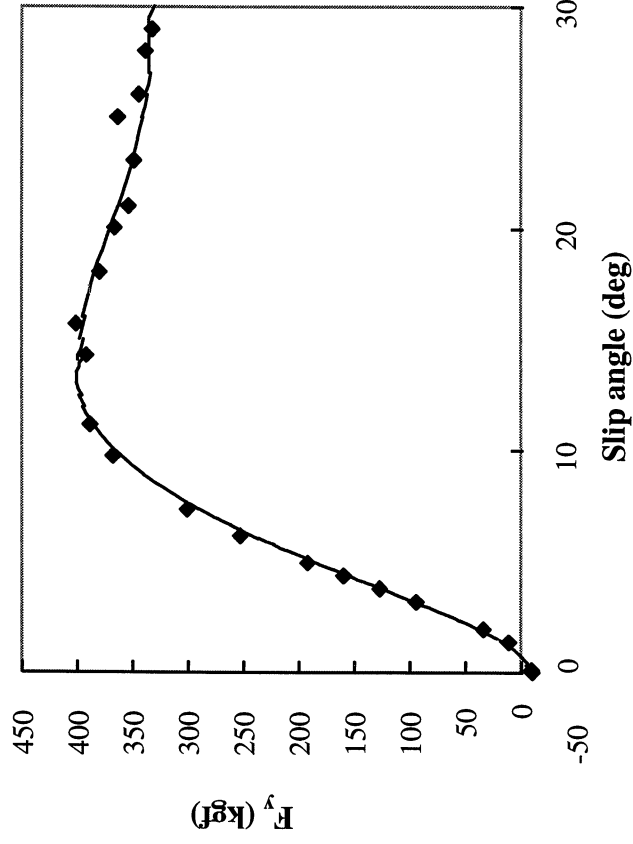


Lateral force measured at transient and steady state

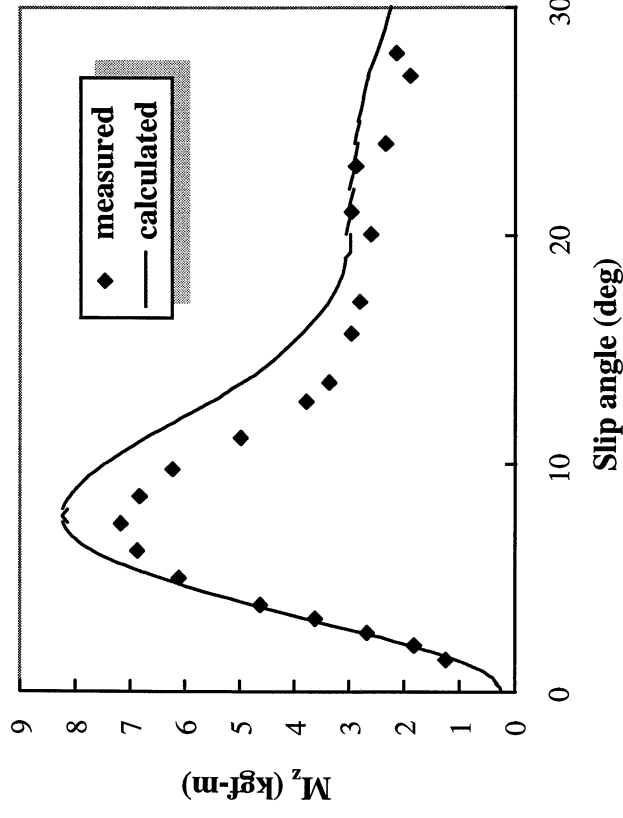


Response of 1st order system for ramp input

Lateral Force/moment at Transient



Lateral force at transient



Self-aligning moment at transient

Conclusions

- **Based on physical Concept**
 - Tire component stiffness
 - Pneumatic trail
 - Pressure distribution
 - Friction ellipse
 - Adhesive contact length
- **Accurate forces/moment for various driving conditions**
 - Load
 - Combined slip
 - Transient