

HYDROELASTIC ANALYSIS OF A RECTANGULAR TANK

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ABSTRACT

A hydroelastic analysis of a rectangular tank is performed using MSC/NASTRAN. Natural frequencies of slosh modes and hydroelastic modes are evaluated, and are compared with results from other approaches as well as analytical values.

INTRODUCTION

Using a MSC/NASTRAN DMAP procedure developed to implement a new fluid-structure formulation [1], a hydroelastic analysis of a liquid-filled rectangular tank is performed. By “hydroelastic” analysis, we are mainly interested in the fluid’s influence on the structural response and not the detailed motion of the fluid.

There are generally two steps in the process of hydroelastic analysis. The first is to calculate the natural frequencies of the slosh modes assuming the rigid tank. The second is to assess the fluid’s influence on the structure. For the slosh modes of the rectangular tank, a few studies have been performed using various approaches [2][3][4]. In this paper, slosh mode frequencies are obtained using a different approach. The results from the approach are compared with corresponding values from other approaches as well as the analytical values. As for the hydroelastic analysis of rectangular tank, not many previous works are readily available. This is in part due to difficulties with estimating the analytical mode frequencies [5]. In this paper, we assume that one pair of facing walls and the bottom of the rectangular tank are rigid, and the remaining pair of facing walls are simply supported. For the hydroelastic modes of the rectangular tank, analytical natural frequencies of the in-phase and out-of-phase modes can be estimated by the energy method [6].

PROBLEM DEFINITION

Consider a rectangular tank, whose geometry is given by the width $a = 0.5$ m, the length $b = 0.7$ m, and the height $h = 0.4$ m, as shown in Figure 1. The topless tank is completely filled with a fluid with the density $\rho = 1000$ Kg/m³. The top surface of the fluid is in a state of free surface. The tank geometry and the fluid property are the same as those in References [2][3][4].

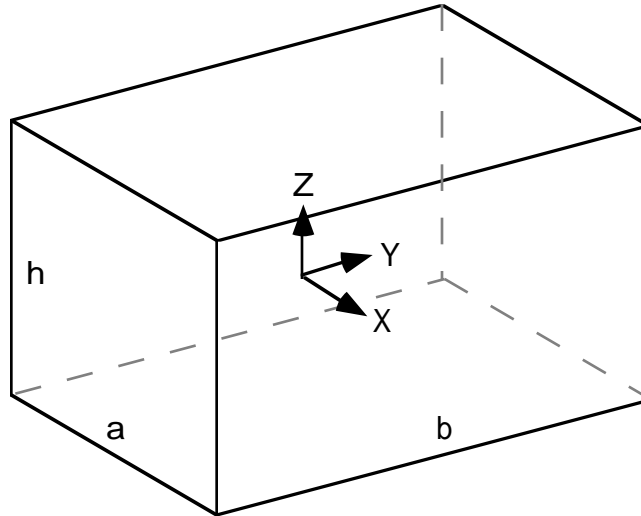


Figure 1: A Rectangular Tank

The rectangular tank has Young’s modulus $E = 2 \times 10^{11}$ pa, Poisson’s ratio $\nu = 0.3$, the thickness $t = 0.005$ m, and the density $\rho_m = 7970$ Kg/m³. The Y-face tank walls and the bottom are considered to be rigid, and the X-face tank walls are assumed to be simply supported. The mesh size for both the fluid and the structure was 0.1 m. The MSC/NASTRAN (V68.2) listing for this problem is included in Appendix.

SLOSH MODE CALCULATIONS

Approaches

In MSC/NASTRAN fluid-structure interaction formulation [2][3], artificial springs are used in defining the free surface stiffness. It also requires artificial plate elements covering the fluid free surface. The formulation is cumbersome, since many bulkdata entries for the artificial springs and plate elements have to be generated. It can be shown that this approach is equivalent to the “mixed” formulation [7], which uses the lumped area formulation for the free surface stiffness matrix and the consistent area formulation in the free surface “mass” matrix.

In the formulation used in this paper [1], slosh modes are calculated using the consistent free surface area matrix [7]. The formulation yields more accurate slosh mode frequencies than the “mixed” formulation using the artificial springs. It also eliminates the need to generate the CELAS2 and CQUAD4 entries.

Area Matrix Calculation

The area matrix calculation involves applying a pressure profile on the surface elements and calculating the resulting loads [8]. For a large fluid-structure interaction problem, this means multiple MSC/NASTRAN static solution runs. Also, thousands of PLOAD4 cards have to be generated [8][9]. In this implementation, MSC/NASTRAN DMAP module ACMG is used to compute the area matrix when the fluid and structure have identical meshes at the interface. Using the ACMG module eliminates the need for PLOAD4 cards and multiple MSC/NASTRAN static solution runs.

Analytical values

The analytical slosh frequencies f_{ij} for the rectangular tank are given by [10]

$$f_{ij}^2 = \frac{g}{4\pi} \sqrt{\left(\frac{i}{a}\right)^2 + \left(\frac{j}{b}\right)^2} \cdot \tanh \left[\pi h \sqrt{\left(\frac{i}{a}\right)^2 + \left(\frac{j}{b}\right)^2} \right] \quad (1)$$

where the gravity constant $g = 10 \text{ m/sec}^2$ and i, j are the mode numbers in the X and Y directions, respectively.

Comparison of Slosh Frequencies

The slosh frequencies of the rectangular tank from the current procedure are compared with the corresponding analytical values and values from other references in Table 1. The Reference [4] values were for $g = 9.8 \text{ m/sec}^2$, and were scaled accordingly in the table. A slosh mode shape corresponding to $i = 1, j = 1$ is shown in Figure 2. The table shows that the results from the current approach are more accurate than those using the “mixed” formulation [2][3] and the HYDRO/BEAMER approach [4]. The mesh sizes used in all approaches were the same.

Table 1. Slosh Frequencies in Rigid Rectangular Tank (in Hz)

Mode		Analytical	Current Procedure	Reference [2][3]	Reference [4]
i	j				
0	0	0.000	0.000		
0	1	1.037	1.048	1.065	1.068
1	0	1.253	1.276	1.318	1.327
1	1	1.396	1.423	1.496	1.525
0	2	1.507	1.559	1.667	1.694
1	2	1.666	1.732	1.914	1.989
2	0	1.784	1.908	2.175	
2	1	1.838	1.967	2.280	
0	3	1.847	1.994	2.317	
1	3	1.940	2.100	2.521	
2	2	1.978	2.136	2.604	

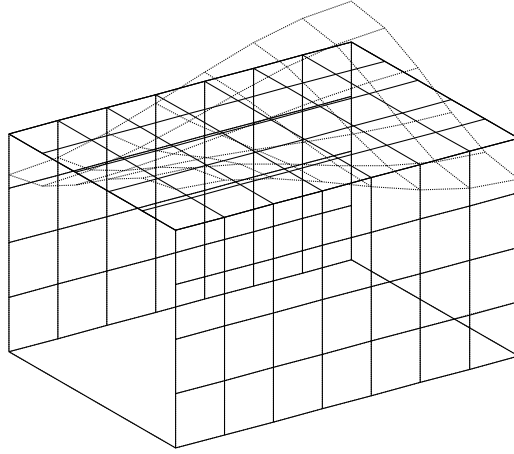


Figure 2: Slosh Mode Shape Corresponding to $i = 1$ and $j = 1$

HYDROELASTIC MODES

Empty Tank

The empty tank modes (simply supported plates) were calculated using MSC/NASTRAN. In Table 2, the natural frequencies of the empty tank modes are compared with the analytical frequencies given by [11]

$$f_{jk} = \frac{\pi}{2} \left\{ \left(\frac{j}{b} \right)^2 + \left(\frac{k}{h} \right)^2 \right\} \sqrt{\frac{Et^2}{12\rho_m(1-\nu^2)}} \quad (2)$$

where j and k are the mode numbers in the Y and Z directions.

Table 2. Natural Frequencies of Empty Rectangular Tank (in Hz)

Mode Shape		Analytical	NASTRAN
j	k		
1	1	98.7	102.5
2	1	171.6	180.6
3	1	293.1	330.4
1	2	322.0	390.6

Analytical results for Hydroelastic Modes

Kito developed formula for the hydroelastic mode frequencies of the rectangular tank using the energy method [6]. For the rectangular tank in consideration, we have

$$\frac{\omega^2 h}{g} \gg 1 \quad (3)$$

where ω is the circular natural frequency of the free vibration of the simply supported plates.

(a) In-phase mode

The side walls are assumed to vibrate in-phase with the mode shape given by

$$w = W \sin my \sin sz \sin \omega t, \quad m = \frac{\pi}{b}, \quad s = \frac{\pi}{h} \quad (4)$$

and the kinetic energy per each wall is given by

$$T_m = \frac{1}{2} [W \cos \omega t]^2 M_{mv} \quad (5)$$

where

$$M_{mv} = \frac{1}{4} M_m = \frac{1}{4} \rho_m t b h \quad (6)$$

The kinetic energy of the fluid allotted to one side wall is given by

$$T_w = \frac{1}{2} [W \omega \cos \omega t]^2 M_{wv} \quad (7)$$

where $M_{wv} = \rho_w V \bar{M}$ is a factor, and $V = a b h$ is the volume of the tank, and the coefficient of virtual mass \bar{M} is given by

$$\bar{M} = \frac{4}{\pi^2} \sum_i \sum_j \left\{ \frac{1}{(i^2 - 1)(j^2 - 1)} \right\}^2 \epsilon \frac{\tanh\left(\frac{1}{2} n_{ij} a\right)}{n_{ij} a} \quad \left(i = 0, 2, 4, \dots; j = \frac{1}{2}, \frac{3}{2}, \frac{5}{2}, \dots \right) \quad (8)$$

where $\epsilon = 4$ if $i \neq 0$, but $\epsilon = 2$ if $i = 0$, and

$$n_{ij}a = \pi \sqrt{\left(\frac{ia}{b}\right)^2 + \left(\frac{ja}{h}\right)^2} \quad (9)$$

Let the frequency of free vibration of the wall be denoted by f and the frequency of free vibration of the same wall in contact with water be denoted by f' . Then the energy method gives

$$f' = \frac{f}{\sqrt{1+\lambda}}, \quad \lambda = \frac{M_{wv}}{M_{mv}} \quad (10)$$

(b) Out-of-phase mode

The out-of-phase mode in which the two facing walls are vibrating in opposite phase is treated in a similar manner. The coefficient of virtual mass \bar{M} for this case is given by

$$\bar{M} = \frac{4}{\pi^2} \sum_i \sum_j \left\{ \frac{1}{(i^2-1)(j^2-1)} \right\}^2 \epsilon \frac{\coth\left(\frac{1}{2}n_{ij}a\right)}{n_{ij}a} \quad \left(i = 0, 2, 4, \dots; \quad j = \frac{1}{2}, \frac{3}{2}, \frac{5}{2}, \dots \right) \quad (11)$$

By using the coefficient of virtual mass, equation (11), in the formula in the previous section, the natural frequency of the out-of-phase mode is similarly obtained. Comparing equations (8) and (11), the virtual mass for the out-of-phase mode is greater than that for the in-phase mode, since for any positive value of x ,

$$\coth x > \tanh x \quad (12)$$

Consequently, the natural frequency for the out-of-phase mode is lower than that for the in-phase mode.

Numerical results for Hydroelastic Modes

The first two coupled fluid-structure mode frequencies are listed in Table 3. The out-of-phase and in-phase modes of the fluid-filled rectangular tank correspond to the empty tank mode with $j = 1, k = 1$, and are shown in Figures 3 and 4, respectively. The frequency for the out-of-phase mode is indeed lower than that for the in-phase mode. The slosh frequencies for the coupled fluid-structure model were almost the same as the rigid container slosh frequencies listed in Table 1, and are not included in Table 3. The table also shows the analytical frequencies by the energy method, as discussed above. The coupled fluid-structure frequencies are in reasonable agreement with the corresponding analytical frequencies by the energy method, considering the coarse meshes used.

Table 3. Hydroelastic Mode Frequencies of Liquid-Filled Rectangular Tank (in Hz)

Mode Shape	Energy Method	Current Approach
In-phase	45.5	49.8
Out-of-phase	37.7	42.2

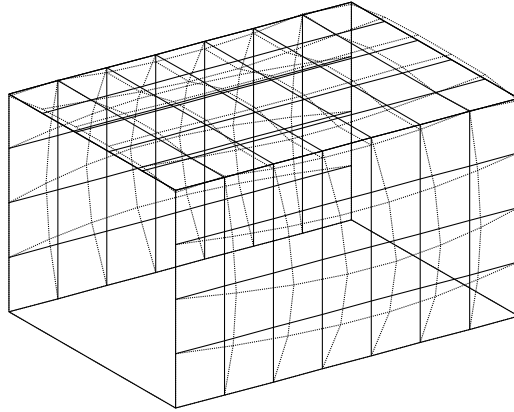


Figure 3: Out-of-phase Rectangular Tank Structure Mode

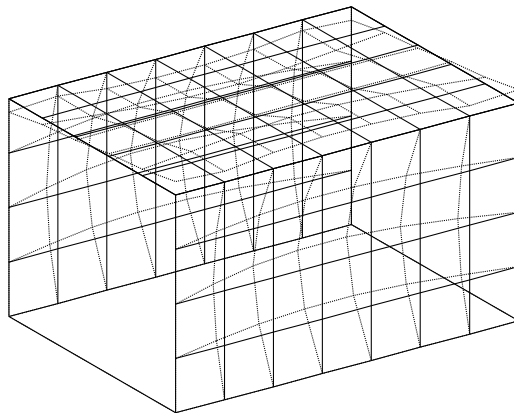


Figure 4: In-phase Rectangular Tank Structure Mode

CONCLUDING REMARKS

This paper presented a hydroelastic analysis of a rectangular tank. A new fluid-structure interaction formulation using a MSC/NASTRAN DMAP program has been used. It has been shown that the implementation is concise and efficient. Also, when compared with various formulations and analytical results, the slosh frequencies obtained using the formulation are more accurate than other approaches. In addition, hydroelastic modes of the rectangular tank are calculated and compared with analytical results obtained using the energy method.

The procedure used in this paper provides insight into hydroelastic analysis of fluid-structure interaction problems. We hope that the attached MSC/NASTRAN input listing would be beneficial to analysts who want to start in the area of fluid-structure interaction.

REFERENCES

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APPENDIX. MSC/NASTRAN LISTING FOR A RECTANGULAR TANK

```
NASTRAN
ASSIGN MASTER ='mesh1.MASTER',TEMP
ASSIGN DBALL ='mesh1.DBALL',TEMP
ASSIGN USRSOU ='mesh1.USRSOU',TEMP
ASSIGN USROBJ ='mesh1.USROBJ',TEMP
INIT DBALL,LOGICAL=(DBALL(50000))
$
ID TEST,NAST
SOL 103
TIME 135
DIAG 8,13
INCLUDE 'hydro_msc.dmap'
CEND
$
TITLE = LIQUID FILLED RECTANGULAR TANK WITH TWO FLEXIBLE SIDE WALLS
$
SPC = 2000
METHOD(FLUID) = 5
METHOD(STRUCTURE) = 10
SET 99 = 20000 THRU 30457
DISP = 99
$
OUTPUT(PLOT)
PLOTTER=NAST
CSCALE=1.5
PAPER SIZE 23.0 BY 28.0
SET 1=ALL
SET 2=PLOTEL
SET 3=PLOTEL,CQUAD4
PTITLE= RECTANGULAR TANK
$
AXES X,Y,Z
VIEW 34.27,23.17,90.
MAXIMUM DEFORMATION 0.075
FIND SCALE,ORIGIN 1,SET 1
FIND SCALE,ORIGIN 2,SET 2
FIND SCALE,ORIGIN 3,SET 3
$PLOT SET 1,ORIGIN 1
$PLOT SET 1,ORIGIN 1,LABEL GRID POINTS,SHAPE
$PLOT SET 1,ORIGIN 1,LABEL ELEMENTS,SHRINK,SHAPE
PLOT MODAL DEFORMATION 0, 1 THRU 52, PEN 2,SET 1, ORIGIN 1$
$
$
BEGIN BULK
$
$
PARAM, NEWSEQ -1
PARAM GRDPNT 0
PARAM USETPRT 0
PARAM COUPMASS 1
PARAM AUTOSPC YES
```

```

PARAM DENSITY 1000.
PARAM GRAVITY 10.
$
$ STRUCTURAL DOFS ( FREE )
$
SPC1      2000  12456  20400  THRU  20457
$
$ STRUCTURAL DOFS ( WETTED )
$
SPC1      2000  23      30000  30007  30050  30057
SPC1      2000  23      30400  30407  30450  30457
SPC1      2000  1       30000  THRU   30057
SPC1      2000  1       30400  THRU   30457
SPC1      2000  1       30100  30200  30300
SPC1      2000  1       30107  30207  30307
SPC1      2000  1       30150  30250  30350
SPC1      2000  1       30157  30257  30357
$
SPC1      2000  4       30000  THRU   30457
$
$ FLUID DOFS ( FREE )
$
CSET1          10400  THRU  10457
$
$ FLUID DOFS ( WETTED )
$
BSET1          10101  THRU  10106
BSET1          10151  THRU  10156
BSET1          10201  THRU  10206
BSET1          10251  THRU  10256
BSET1          10301  THRU  10306
BSET1          10351  THRU  10356
$
$ STRUCTURAL DOFS (WETTED)
$
BSET1      1      30101  THRU  30106
BSET1      1      30201  THRU  30206
BSET1      1      30301  THRU  30306
BSET1      1      30151  THRU  30156
BSET1      1      30251  THRU  30256
BSET1      1      30351  THRU  30356
$
$ STRUCTURAL DOFS (FLUID SLOSH MODES)
$
QSET1      3      20400  THRU  20457
$
$ Definition of fluid nodes in the wetted and free surface areas
$
SET1      100      10400  THRU  10445  10446  10447  10450  10451  +ST11
+ST11    10000  THRU  10007  10050  THRU  10057  10452  10453  +ST12
+ST12    10100  THRU  10107  10150  THRU  10157  10454  10455  +ST13
+ST13    10200  THRU  10207  10250  THRU  10257  10456  10457  +ST14
+ST14    10300  THRU  10307  10350  THRU  10357
$

```

\$ Definition of structural nodes in the wetted and free surface areas

\$

SET1	200	20400	THRU	20445	20446	20447	20450	20451	+ST21
+ST21	30000	THRU	30007	30050	THRU	30057	20452	20453	+ST22
+ST22	30100	THRU	30107	30150	THRU	30157	20454	20455	+ST23
+ST23	30200	THRU	30207	30250	THRU	30257	20456	20457	+ST24
+ST24	30300	THRU	30307	30350	THRU	30357			

\$

ACMODL	IDENT	ALL	100	200
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GRID	10405	-.25	.15	.2
GRID	10406	-.25	.25	.2
GRID	10407	-.25	.35	.2
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GRID	10411	-.15	-.25	.2
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CHEXA	103	10	10244	10245	10255	10254	10344	10345	+M00102	
+M00102	10355	10354								
CHEXA	104	10	10245	10246	10256	10255	10345	10346	+M00103	
+M00103	10356	10355								
CHEXA	105	10	10246	10247	10257	10256	10346	10347	+M00104	
+M00104	10357	10356								
CHEXA	106	10	10300	10301	10311	10310	10400	10401	+M00105	
+M00105	10411	10410								
CHEXA	107	10	10301	10302	10312	10311	10401	10402	+M00106	

+M00106	10412	10411								
CHEXA	108	10	10302	10303	10313	10312	10402	10403	+M00107	
+M00107	10413	10412								
CHEXA	109	10	10303	10304	10314	10313	10403	10404	+M00108	
+M00108	10414	10413								
CHEXA	110	10	10304	10305	10315	10314	10404	10405	+M00109	
+M00109	10415	10414								
CHEXA	111	10	10305	10306	10316	10315	10405	10406	+M00110	
+M00110	10416	10415								
CHEXA	112	10	10306	10307	10317	10316	10406	10407	+M00111	
+M00111	10417	10416								
CHEXA	113	10	10310	10311	10321	10320	10410	10411	+M00112	
+M00112	10421	10420								
CHEXA	114	10	10311	10312	10322	10321	10411	10412	+M00113	
+M00113	10422	10421								
CHEXA	115	10	10312	10313	10323	10322	10412	10413	+M00114	
+M00114	10423	10422								
CHEXA	116	10	10313	10314	10324	10323	10413	10414	+M00115	
+M00115	10424	10423								
CHEXA	117	10	10314	10315	10325	10324	10414	10415	+M00116	
+M00116	10425	10424								
CHEXA	118	10	10315	10316	10326	10325	10415	10416	+M00117	
+M00117	10426	10425								
CHEXA	119	10	10316	10317	10327	10326	10416	10417	+M00118	
+M00118	10427	10426								
CHEXA	120	10	10320	10321	10331	10330	10420	10421	+M00119	
+M00119	10431	10430								
CHEXA	121	10	10321	10322	10332	10331	10421	10422	+M00120	
+M00120	10432	10431								
CHEXA	122	10	10322	10323	10333	10332	10422	10423	+M00121	
+M00121	10433	10432								
CHEXA	123	10	10323	10324	10334	10333	10423	10424	+M00122	
+M00122	10434	10433								
CHEXA	124	10	10324	10325	10335	10334	10424	10425	+M00123	
+M00123	10435	10434								
CHEXA	125	10	10325	10326	10336	10335	10425	10426	+M00124	
+M00124	10436	10435								
CHEXA	126	10	10326	10327	10337	10336	10426	10427	+M00125	
+M00125	10437	10436								
CHEXA	127	10	10330	10331	10341	10340	10430	10431	+M00126	
+M00126	10441	10440								
CHEXA	128	10	10331	10332	10342	10341	10431	10432	+M00127	
+M00127	10442	10441								
CHEXA	129	10	10332	10333	10343	10342	10432	10433	+M00128	
+M00128	10443	10442								
CHEXA	130	10	10333	10334	10344	10343	10433	10434	+M00129	
+M00129	10444	10443								
CHEXA	131	10	10334	10335	10345	10344	10434	10435	+M00130	
+M00130	10445	10444								
CHEXA	132	10	10335	10336	10346	10345	10435	10436	+M00131	
+M00131	10446	10445								
CHEXA	133	10	10336	10337	10347	10346	10436	10437	+M00132	
+M00132	10447	10446								
CHEXA	134	10	10340	10341	10351	10350	10440	10441	+M00133	

+M00133	10451	10450							
CHEXA	135	10	10341	10342	10352	10351	10441	10442	+M00134
+M00134	10452	10451							
CHEXA	136	10	10342	10343	10353	10352	10442	10443	+M00135
+M00135	10453	10452							
CHEXA	137	10	10343	10344	10354	10353	10443	10444	+M00136
+M00136	10454	10453							
CHEXA	138	10	10344	10345	10355	10354	10444	10445	+M00137
+M00137	10455	10454							
CHEXA	139	10	10345	10346	10356	10355	10445	10446	+M00138
+M00138	10456	10455							
CHEXA	140	10	10346	10347	10357	10356	10446	10447	+M00139
+M00139	10457	10456							
\$									
PSOLID	10	10							PFLUID
MAT10	10		1000.	1524.					
\$									
PSHELL	20	20	0.001	20					
MAT1	20	1.-3		0.3					
\$									
CQUAD4	301	30	30000	30001	30101	30100			
CQUAD4	302	30	30001	30002	30102	30101			
CQUAD4	303	30	30002	30003	30103	30102			
CQUAD4	304	30	30003	30004	30104	30103			
CQUAD4	305	30	30004	30005	30105	30104			
CQUAD4	306	30	30005	30006	30106	30105			
CQUAD4	307	30	30006	30007	30107	30106			
CQUAD4	308	30	30100	30101	30201	30200			
CQUAD4	309	30	30101	30102	30202	30201			
CQUAD4	310	30	30102	30103	30203	30202			
CQUAD4	311	30	30103	30104	30204	30203			
CQUAD4	312	30	30104	30105	30205	30204			
CQUAD4	313	30	30105	30106	30206	30205			
CQUAD4	314	30	30106	30107	30207	30206			
CQUAD4	315	30	30200	30201	30301	30300			
CQUAD4	316	30	30201	30202	30302	30301			
CQUAD4	317	30	30202	30203	30303	30302			
CQUAD4	318	30	30203	30204	30304	30303			
CQUAD4	319	30	30204	30205	30305	30304			
CQUAD4	320	30	30205	30206	30306	30305			
CQUAD4	321	30	30206	30207	30307	30306			
CQUAD4	322	30	30300	30301	30401	30400			
CQUAD4	323	30	30301	30302	30402	30401			
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CQUAD4	325	30	30303	30304	30404	30403			
CQUAD4	326	30	30304	30305	30405	30404			
CQUAD4	327	30	30305	30306	30406	30405			
CQUAD4	328	30	30306	30307	30407	30406			
CQUAD4	351	30	30050	30051	30151	30150			
CQUAD4	352	30	30051	30052	30152	30151			
CQUAD4	353	30	30052	30053	30153	30152			
CQUAD4	354	30	30053	30054	30154	30153			
CQUAD4	355	30	30054	30055	30155	30154			
CQUAD4	356	30	30055	30056	30156	30155			

CQUAD4	357	30	30056	30057	30157	30156
CQUAD4	358	30	30150	30151	30251	30250
CQUAD4	359	30	30151	30152	30252	30251
CQUAD4	360	30	30152	30153	30253	30252
CQUAD4	361	30	30153	30154	30254	30253
CQUAD4	362	30	30154	30155	30255	30254
CQUAD4	363	30	30155	30156	30256	30255
CQUAD4	364	30	30156	30157	30257	30256
CQUAD4	365	30	30250	30251	30351	30350
CQUAD4	366	30	30251	30252	30352	30351
CQUAD4	367	30	30252	30253	30353	30352
CQUAD4	368	30	30253	30254	30354	30353
CQUAD4	369	30	30254	30255	30355	30354
CQUAD4	370	30	30255	30256	30356	30355
CQUAD4	371	30	30256	30257	30357	30356
CQUAD4	372	30	30350	30351	30451	30450
CQUAD4	373	30	30351	30352	30452	30451
CQUAD4	374	30	30352	30353	30453	30452
CQUAD4	375	30	30353	30354	30454	30453
CQUAD4	376	30	30354	30355	30455	30454
CQUAD4	377	30	30355	30356	30456	30455
CQUAD4	378	30	30356	30357	30457	30456
\$						
PSHELL	30	30	0.005	30		
MAT1	30	2.0+11		0.3	7.97+3	
\$						
PLOTEL	201	20400	20401			
PLOTEL	202	20401	20402			
PLOTEL	203	20402	20403			
PLOTEL	204	20403	20404			
PLOTEL	205	20404	20405			
PLOTEL	206	20405	20406			
PLOTEL	207	20406	20407			
PLOTEL	208	20410	20411			
PLOTEL	209	20411	20412			
PLOTEL	210	20412	20413			
PLOTEL	211	20413	20414			
PLOTEL	212	20414	20415			
PLOTEL	213	20415	20416			
PLOTEL	214	20416	20417			
PLOTEL	215	20420	20421			
PLOTEL	216	20421	20422			
PLOTEL	217	20422	20423			
PLOTEL	218	20423	20424			
PLOTEL	219	20424	20425			
PLOTEL	220	20425	20426			
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PLOTEL	223	20431	20432			
PLOTEL	224	20432	20433			
PLOTEL	225	20433	20434			
PLOTEL	226	20434	20435			
PLOTEL	227	20435	20436			
PLOTEL	228	20436	20437			

PLOTEL	229	20440	20441
PLOTEL	230	20441	20442
PLOTEL	231	20442	20443
PLOTEL	232	20443	20444
PLOTEL	233	20444	20445
PLOTEL	234	20445	20446
PLOTEL	235	20446	20447
PLOTEL	236	20450	20451
PLOTEL	237	20451	20452
PLOTEL	238	20452	20453
PLOTEL	239	20453	20454
PLOTEL	240	20454	20455
PLOTEL	241	20455	20456
PLOTEL	242	20456	20457
PLOTEL	251	20400	20410
PLOTEL	252	20410	20420
PLOTEL	253	20420	20430
PLOTEL	254	20430	20440
PLOTEL	255	20440	20450
PLOTEL	256	20401	20411
PLOTEL	257	20411	20421
PLOTEL	258	20421	20431
PLOTEL	259	20431	20441
PLOTEL	260	20441	20451
PLOTEL	261	20402	20412
PLOTEL	262	20412	20422
PLOTEL	263	20422	20432
PLOTEL	264	20432	20442
PLOTEL	265	20442	20452
PLOTEL	266	20403	20413
PLOTEL	267	20413	20423
PLOTEL	268	20423	20433
PLOTEL	269	20433	20443
PLOTEL	270	20443	20453
PLOTEL	271	20404	20414
PLOTEL	272	20414	20424
PLOTEL	273	20424	20434
PLOTEL	274	20434	20444
PLOTEL	275	20444	20454
PLOTEL	276	20405	20415
PLOTEL	277	20415	20425
PLOTEL	278	20425	20435
PLOTEL	279	20435	20445
PLOTEL	280	20445	20455
PLOTEL	281	20406	20416
PLOTEL	282	20416	20426
PLOTEL	283	20426	20436
PLOTEL	284	20436	20446
PLOTEL	285	20446	20456
PLOTEL	286	20407	20417
PLOTEL	287	20417	20427
PLOTEL	288	20427	20437
PLOTEL	289	20437	20447
PLOTEL	290	20447	20457

PLOTEL	296	10000	10050
PLOTEL	297	10400	10450
PLOTEL	298	10007	10057
PLOTEL	299	10407	10457

\$
ENDDATA