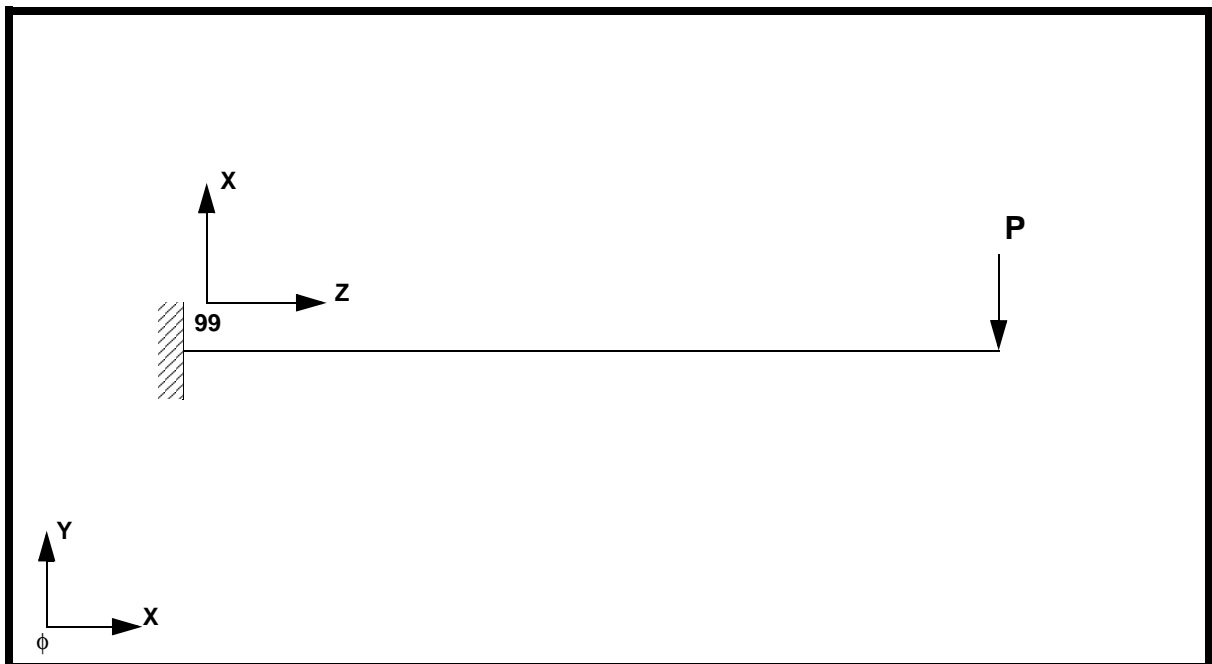


WORKSHOP 12

The Effect of Multiple Coordinate System



Objectives:

- Create a cantilever beam model
- Assign different coordinate systems as reference and displacement coordinate system
- Run an MSC.Nastran Linear Static analysis
- Modify reference and displacement coordinate system
- Compare the analysis results

Model Description:

The goal of this example is to examine the effect of different coordinate systems. A linear static analysis of a cantilever beam will be performed using multiple coordinate systems.

We will examine the following 3 cases

Case 1

Ref. coord. = ϕ

Disp. coord. = ϕ

Case 2

Ref. coord. = 99

Disp. coord. = ϕ

Case 3

Ref. coord. = 99

Disp. coord. = 99

Question:

For case 3, the displacement vectors have been shifted to T1 column. However, are the values correct? What about the SPC force ?

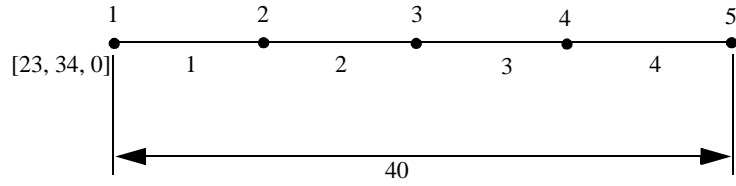


Figure 12.1 - Grid Coordinates and Element Connectivities

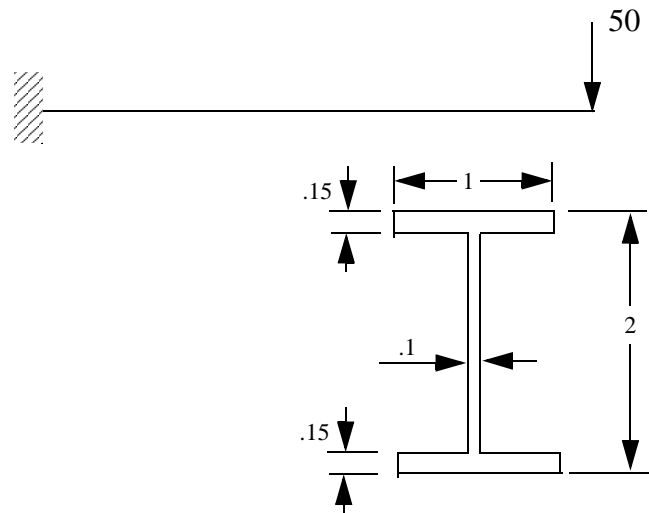


Figure 12.2 - Loads and Boundary Conditions

Suggested Exercise Steps:

- Define a local coordinate system 99
 - Origin
 - Point on Axis 3
 - Point of plane 1-3
- Generate a finite element representation of the cantilever beam. (i.e., The nodes (GRID) and element connectivities (CBAR).
- Use the basic coordinate system, coord. ϕ , as the reference and displacement coordinate systems.
- Define material (MAT1) and the element (PBAR) properties.
- Apply the fix boundary constraints (SPC1) at the left tip.
- Apply the concentrated force of 50lbs (FORCE) at the free end.
- Prepare the model for linear static analysis (SOL 101).
- Review the results.


```

SOL 101
CEND
ECHO = NONE
SUBCASE 1
  SPC = 1
  LOAD = 1
  DISPLACEMENT=ALL
  SPCFORCES=ALL
  STRESS=ALL
BEGIN BULK
PARAM      POST      -1
$
PBARL      1          1          I
+          A
+          A 2.      1.          1.          .1          .15          .15
$
CBAR       1          1          1          2          0.          1.          0.
CBAR       2          1          2          3          0.          1.          0.
CBAR       3          1          3          4          0.          1.          0.
CBAR       4          1          4          5          0.          1.          0.
$
MAT1       1          1.+7          .3
$
GRID       1          23.         34.         0.
GRID       2          33.         34.         0.
GRID       3          43.         34.         0.
GRID       4          53.         34.         0.
GRID       5          63.         34.         0.
$
SPC1       1          123456  1
$
FORCE      1          5          0          50.         0.          -1.          0.
$
ENDDATA

```

Case 1

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	0.0	0.0	0.0	0.0	0.0	0.0
2	G	0.0	-3.150556E-02	0.0	0.0	0.0	-5.868709E-03
3	G	0.0	-1.133143E-01	0.0	0.0	0.0	-1.006064E-02
4	G	0.0	-2.286586E-01	0.0	0.0	0.0	-1.257580E-02
5	G	0.0	-3.607706E-01	0.0	0.0	0.0	-1.341419E-02

FORCES OF SINGLE-POINT CONSTRAINT

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	0.0	5.000000E+01	0.0	0.0	0.0	2.000000E+03

ELEMENT ID.	SA1	SA2	SA3	SA4	STRESSES IN BAR ELEMENTS (C B A R)				SA-MIN	SA-MAX	SB-MIN	SB-MAX	M.S.-T	M.S.-C
					SB1	SB2	SB3	SB4						
0 1	6.707096E+03	-6.707096E+03	-6.707096E+03	6.707096E+03	6.707096E+03	0.0	0.0	0.0	6.707096E+03	-6.707096E+03	-6.707096E+03	6.707096E+03		
0 2	5.030322E+03	-5.030322E+03	-5.030322E+03	5.030322E+03	5.030322E+03	0.0	0.0	0.0	5.030322E+03	-5.030322E+03	-5.030322E+03	5.030322E+03		
0 3	3.353548E+03	-3.353548E+03	-3.353548E+03	3.353548E+03	3.353548E+03	0.0	0.0	0.0	3.353548E+03	-3.353548E+03	-3.353548E+03	3.353548E+03		
0 4	1.676774E+03	-1.676774E+03	-1.676774E+03	1.676774E+03	1.676774E+03	0.0	0.0	0.0	1.676774E+03	-1.676774E+03	-1.676774E+03	1.676774E+03		
	3.050034E-11	-3.050034E-11	-3.050034E-11	3.050034E-11	3.050034E-11				3.050034E-11	-3.050034E-11	-3.050034E-11	3.050034E-11		

```

SOL 101
CEND
ECHO = NONE
SUBCASE 1
  SPC = 1
  LOAD = 1
  DISPLACEMENT=ALL
  SPCFORCES=ALL
  STRESS=ALL
BEGIN BULK
PARAM      POST      -1
$
PBARL      1          1          I
+
  A
+
  A 2.         1.         1.         .1         .15         .15
$
CBAR       1          1          1          2          0.         1.         0.
CBAR       2          1          2          3          0.         1.         0.
CBAR       3          1          3          4          0.         1.         0.
CBAR       4          1          4          5          0.         1.         0.
$
MAT1       1          1.+7          .3
$
GRID       1          99          0.         0.         0.
GRID       2          99          0.         0.         10.
GRID       3          99          0.         0.         20.
GRID       4          99          0.         0.         30.
GRID       5          99          0.         0.         40.
$
SPC1       1          123456 1
$
FORCE      1          5          0          50.        0.         -1.         0.
$
CORD2R     99          23.         34.         0.         24.         34.         0.
+
  B
+
  B 23.        35.         0.
ENDDATA

```

Case 2

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	0.0	0.0	0.0	0.0	0.0	0.0
2	G	0.0	-3.150556E-02	0.0	0.0	0.0	-5.86E709E-03
3	G	0.0	-1.13143E-01	0.0	0.0	0.0	-1.006064E-02
4	G	0.0	-2.285585E-01	0.0	0.0	0.0	-1.257580E-02
5	G	0.0	-3.607706E-01	0.0	0.0	0.0	-1.341419E-02

FORCES OF SINGLE-POINT CONSTRAINT

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	0.0	5.000000E+01	0.0	0.0	0.0	2.000000E+03

SUBCASE 1

ELEMENT ID.	STRESSES IN BAR ELEMENTS				(C B A R)		M.S.-T M.S.-C
	SA1 SB1	SA2 SB2	SA3 SB3	SA4 SB4	SA-MAX SB-MAX	SA-MIN SB-MIN	
0 1	6.707096E+03	-6.707096E+03	-6.707096E+03	6.707096E+03	6.707096E+03	-6.707096E+03	
0 2	5.030322E+03	-5.030322E+03	-5.030322E+03	5.030322E+03	5.030322E+03	-5.030322E+03	
0 3	3.353548E+03	-3.353548E+03	-3.353548E+03	3.353548E+03	3.353548E+03	-3.353548E+03	
0 4	1.67674E+03	-1.67674E+03	-1.67674E+03	1.67674E+03	1.67674E+03	-1.67674E+03	
0 5	3.050034E-11	-3.050034E-11	-3.050034E-11	3.050034E-11	3.050034E-11	-3.050034E-11	

```

SOL 101
CEND
ECHO = NONE
SUBCASE 1
  SPC = 1
  LOAD = 1
  DISPLACEMENT=ALL
  SPCFORCES=ALL
  STRESS=ALL
BEGIN BULK
PARAM      POST      -1
$
PBARL      1          1          I
+          A
+          A 2.       1.         1.         .1         .15         .15
$
CBAR       1          1          1          2          0.         1.         0.
CBAR       2          1          2          3          0.         1.         0.
CBAR       3          1          3          4          0.         1.         0.
CBAR       4          1          4          5          0.         1.         0.
$
MAT1       1          1.+7          .3
$
GRID       1          99          0.         0.         0.         99
GRID       2          99          0.         0.         10.        99
GRID       3          99          0.         0.         20.        99
GRID       4          99          0.         0.         30.        99
GRID       5          99          0.         0.         40.        99
$
SPC1       1          123456      1
$
FORCE      1          5          0          50.        0.         -1.         0.
$
CORD2R     99          23.        34.        0.         24.        34.        0.
+          B
+          B 23.      35.        0.
ENDDATA

```

Case 3

DISPLACEMENT VECTOR

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	0.0	0.0	0.0	0.0	0.0	0.0
2	G	-3.651206E-01	0.0	0.0	0.0	-6.960557E-02	0.0
3	G	-1.326860E+00	0.0	0.0	0.0	-1.193238E-01	0.0
4	G	-2.686346E+00	0.0	0.0	0.0	-1.491548E-01	0.0
5	G	-4.244705E+00	0.0	0.0	0.0	-1.590984E-01	0.0

FORCES OF SINGLE-POINT CONSTRAINT

POINT ID.	TYPE	T1	T2	T3	R1	R2	R3
1	G	5.000000E+01	0.0	0.0	0.0	2.000000E+03	0.0

ELEMENT ID.	SA1		SA2		SA3		SA4		S T R E S S E S I N B A R E L E M E N T S		(C B A R)		M.S.-T	
	SB1	SB2	SB3	SB4	SB5	SB6	SB7	SB8	AXIAL STRESS	SA-MAX	SB-MAX	SA-MIN	SB-MIN	M.S.-C
0	1	-3.977461E+04	-3.977461E+04	3.977461E+04	3.977461E+04	3.977461E+04	3.977461E+04	3.977461E+04	0.0	3.977461E+04	3.977461E+04	-3.977461E+04	-3.977461E+04	
0	2	-2.983096E+04	-2.983096E+04	2.983096E+04	2.983096E+04	2.983096E+04	2.983096E+04	2.983096E+04	0.0	2.983096E+04	2.983096E+04	-2.983096E+04	-2.983096E+04	
0	3	-1.988730E+04	-1.988730E+04	1.988730E+04	1.988730E+04	1.988730E+04	1.988730E+04	1.988730E+04	0.0	1.988730E+04	1.988730E+04	-1.988730E+04	-1.988730E+04	
0	4	-9.943652E+03	-9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	0.0	9.943652E+03	9.943652E+03	-9.943652E+03	-9.943652E+03	
0	4	-9.943652E+03	-9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	9.943652E+03	0.0	9.943652E+03	9.943652E+03	-9.943652E+03	-9.943652E+03	
0	4	-3.617480E-10	-3.617480E-10	3.617480E-10	3.617480E-10	3.617480E-10	3.617480E-10	3.617480E-10	0.0	3.617480E-10	3.617480E-10	-3.617480E-10	-3.617480E-10	